

Chapter 7: Gas-Phase Concentration measurement

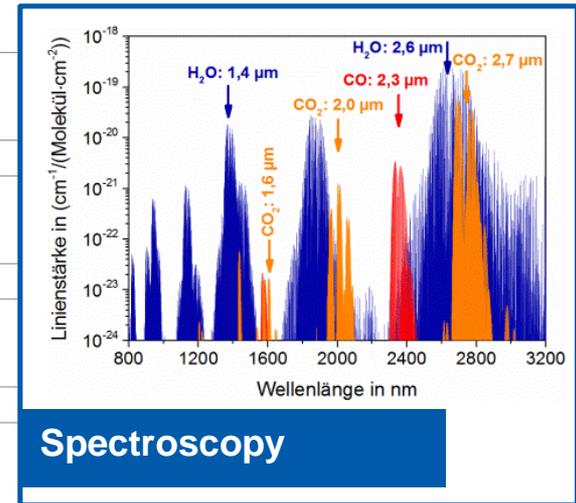
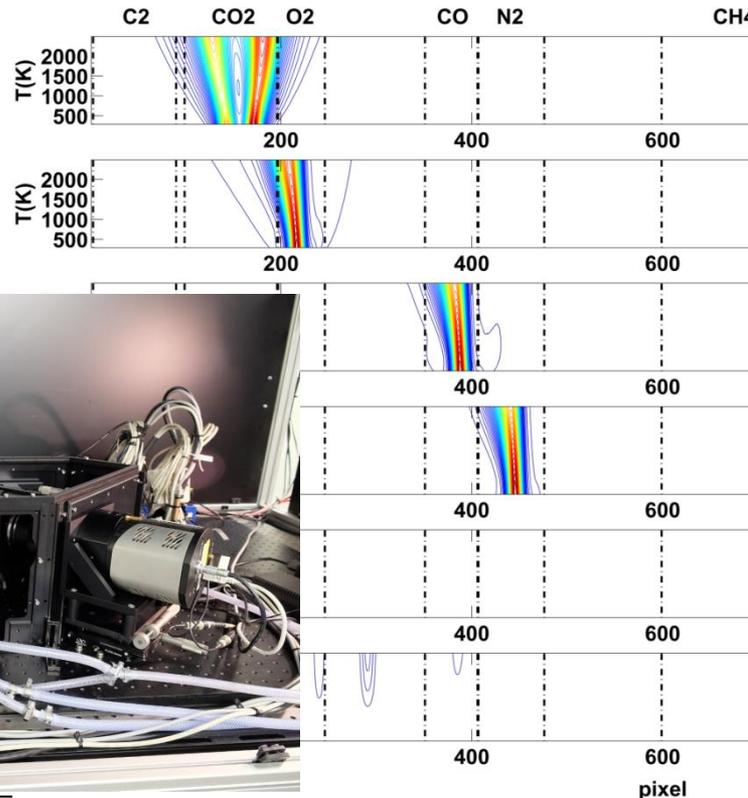
TU Darmstadt, Germany
Dept. of Mechanical Engineering
Institute for Reactive Flows and Diagnostics



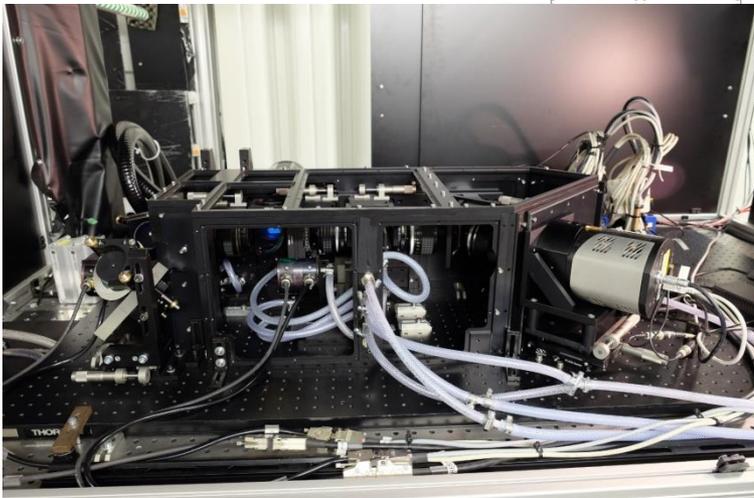
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A. Dreizler



Spectroscopy



Motivation for quantitative species concentration measurement

- Quantitative concentration measurements are motivated by various scientific and technological issues
- Target species depends on the combustion process
 - Mixture fraction
 - Reaction progress and intermediate species concentration
 - Pollutants
 - ...
- A quantitative species measurement in combustion application requires information of local gas temperature (density correction and method-related correction such as quenching correction in LIF)
 - Best option: measure simultaneously local temperature

Methods in the NIR/UV/VIS for temperature measurements via Boltzmann distribution

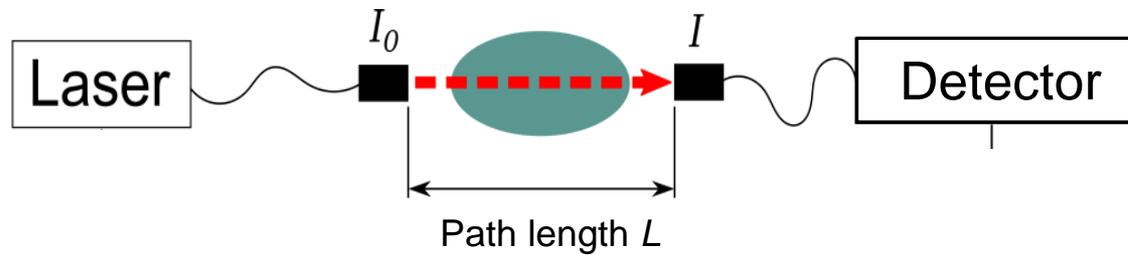


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- Laser absorption spectroscopy (LAS)
- Laser-induced fluorescence (LIF)
- Raman spectroscopy (RS)

Laser absorption spectroscopy (1)

- Experimental setup



- Deduce number densities from Beer-Lambert's law (shown in its simplest form)

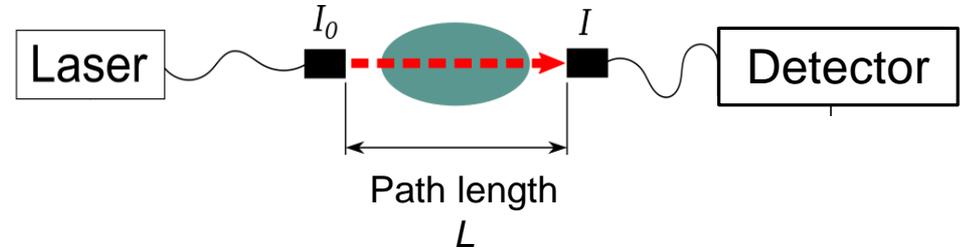
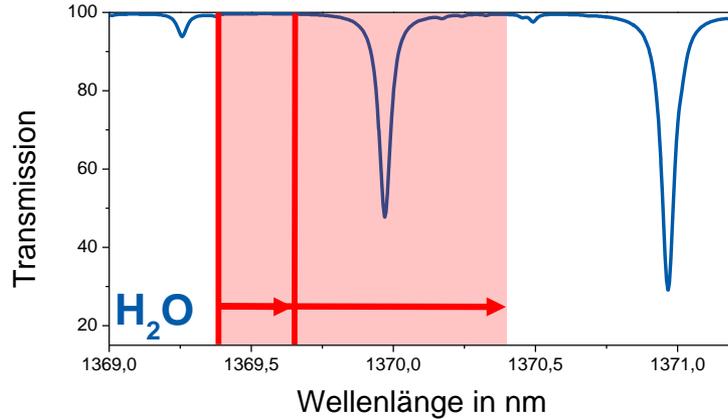
$$I(L) = I_0 \exp(-L \cdot N_J \cdot \sigma_{j \leftarrow i}) \Leftrightarrow N_J = \frac{\ln\left(\frac{I(L)}{I_0}\right)}{L \cdot \sigma_{j \leftarrow i}}$$

Calibration free (once the path length and absorption cross-section is known)

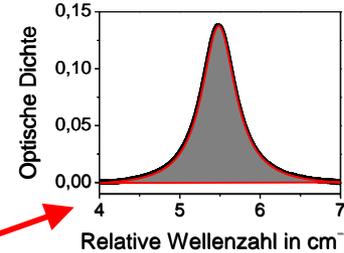
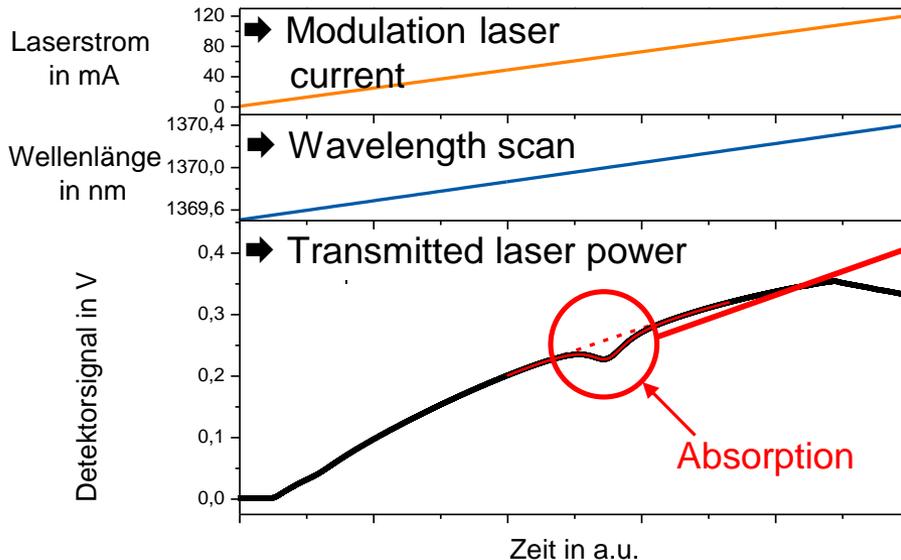
Line-of-sight: no resolution along laser beam path

→ restrictions for application in turbulent flames

Tuneable diode laser absorption spectroscopy TDLAS



Lambert-Beer-law



Ideal gas law
↓
species concentration

$$c = \frac{k_B \cdot T}{S(T) \cdot L \cdot p} \int \ln \left(\frac{I_0(\nu)}{I(\nu)} \right) \frac{d\nu}{dt} dt$$

Laser Induced fluorescence: Principle

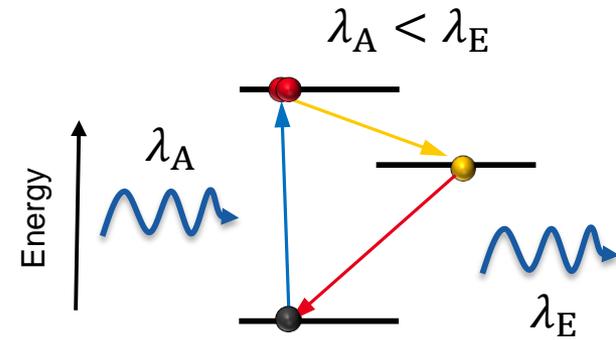
Step 1: Absorption

- Electronic excitation of molecules by laser radiation
- Wavelength λ_A

Step 2: Spontaneous emission (fluorescence)

- Spectrally red-shifted $\lambda_A < \lambda_E$
- Upper state lifetime few ns
- Measure of local number density

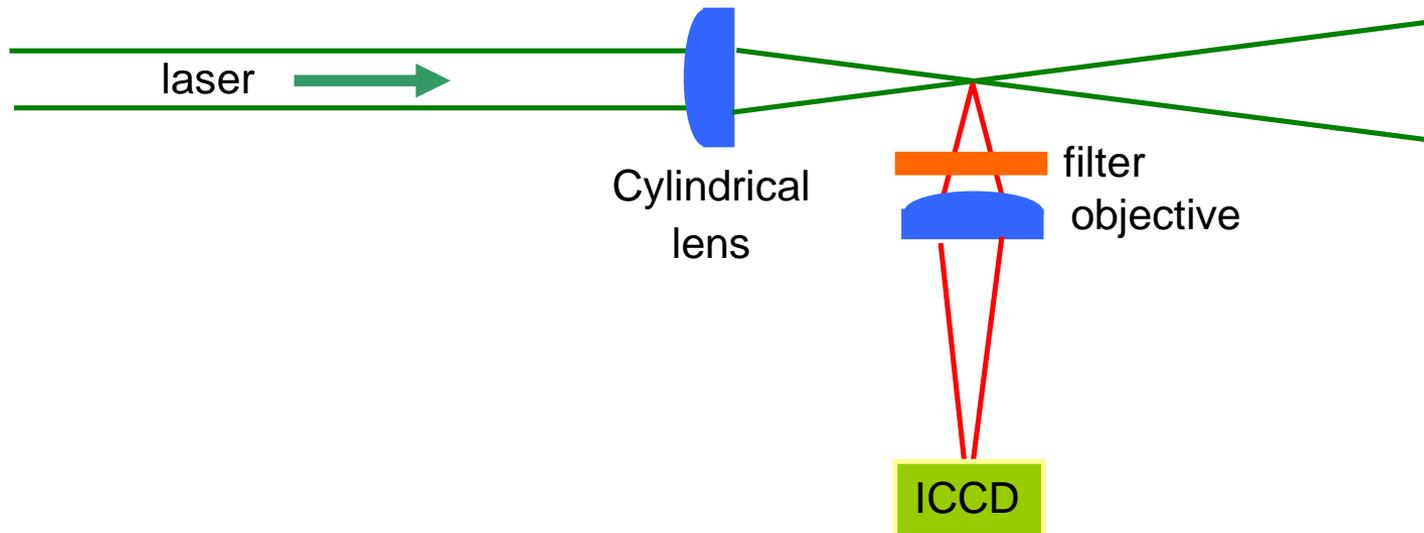
- Linear LIF regime



$$I_{LIF}(x) = N_1(x) \sigma \gamma(\nu) I_{laser}(x) \frac{\tau_{tot}}{\tau_{sp}} U \frac{\Omega}{4\pi} \varepsilon \eta$$

Laser Induced fluorescence: Experimental setup

- Experimental setup



Laser Induced fluorescence: pros and cons



- Good spatial resolution (90° detection angle)
- Sensitive
- Calibration required to determine $U \frac{\Omega}{4\pi} \varepsilon \eta$
- Total lifetime τ_{tot} needed but often not known!

$$I_{LIF}(x) = N_1(x) \sigma \gamma(\nu) I_{laser}(x) \frac{\tau_{tot}}{\tau_{sp}} U \frac{\Omega}{4\pi} \varepsilon \eta$$

$$\tau_{tot} = \frac{1}{A + P + Q}$$

A : Einstein A-coefficient, molecular property, often known

P : Predissociation rate, molecular property, often known

Q : Quenching rate, depends on gas matrix, pressure, temperature → PROBLEM

Total lifetime τ_{tot} makes quantitative LIF challenging!

How to make LIF quantitative – options

1. Quantification of τ_{tot} : Measure $\tau_{\text{tot}} = \text{fct}(T, \text{species})$,
once $\tau_{\text{tot}}(T, \text{species})$ is known measure LIF simultaneously with T and
species (via Raman/Rayleigh)
2. Calibration: determine $C = C(T)$ in $I_{\text{LIF}}(x) = C(T)[N_1(x)]$
→Example CO-LIF in application example flame-wall interaction
3. Saturated LIF: does not really work, not detailed here
4. Combine 1D-LIF with absorption spectroscopy (see CST 158, 2000,
Pixner et al.)

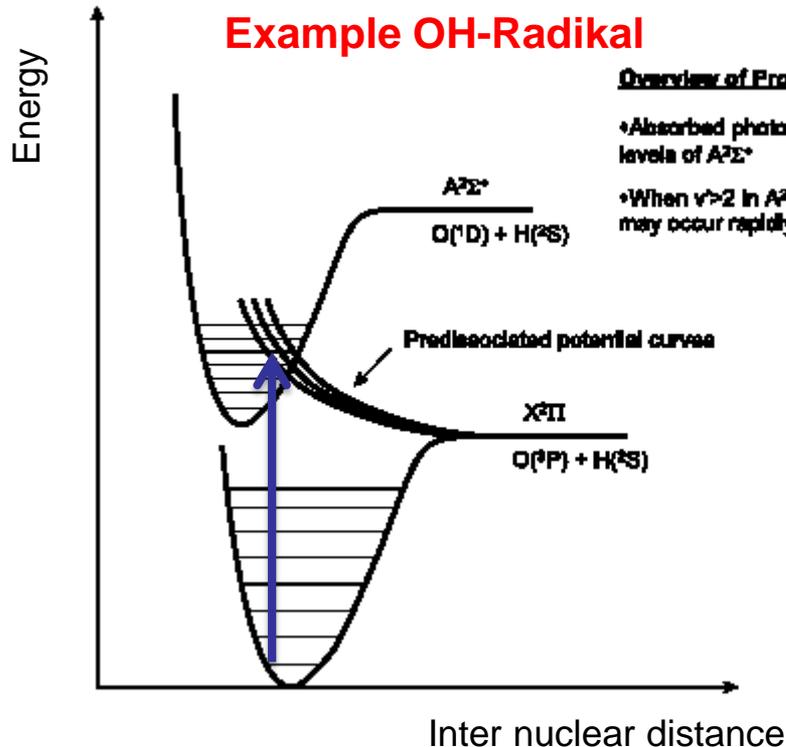
$$N_1(x) = -\frac{1}{\sigma} \cdot \frac{(T-1) \frac{dV(x)}{dx}}{(T-1)V(x) + 1}$$

$$V(x) = \frac{\int_0^x F(x') dx'}{\int_0^L F(x') dx'} = \frac{\exp\left(-\sigma \int_0^x N_1(x') dx'\right) - 1}{\exp\left(-\sigma \int_0^L N_1(x') dx'\right) - 1}$$

$$T = \frac{I(L)}{I(0)} = \exp\left(-\sigma \int_0^L N_1(x') dx'\right)$$

How to make LIF quantitative – options

5. Predissociative LIF: Independent of Q; low SNR, works for few molecules at low pressure

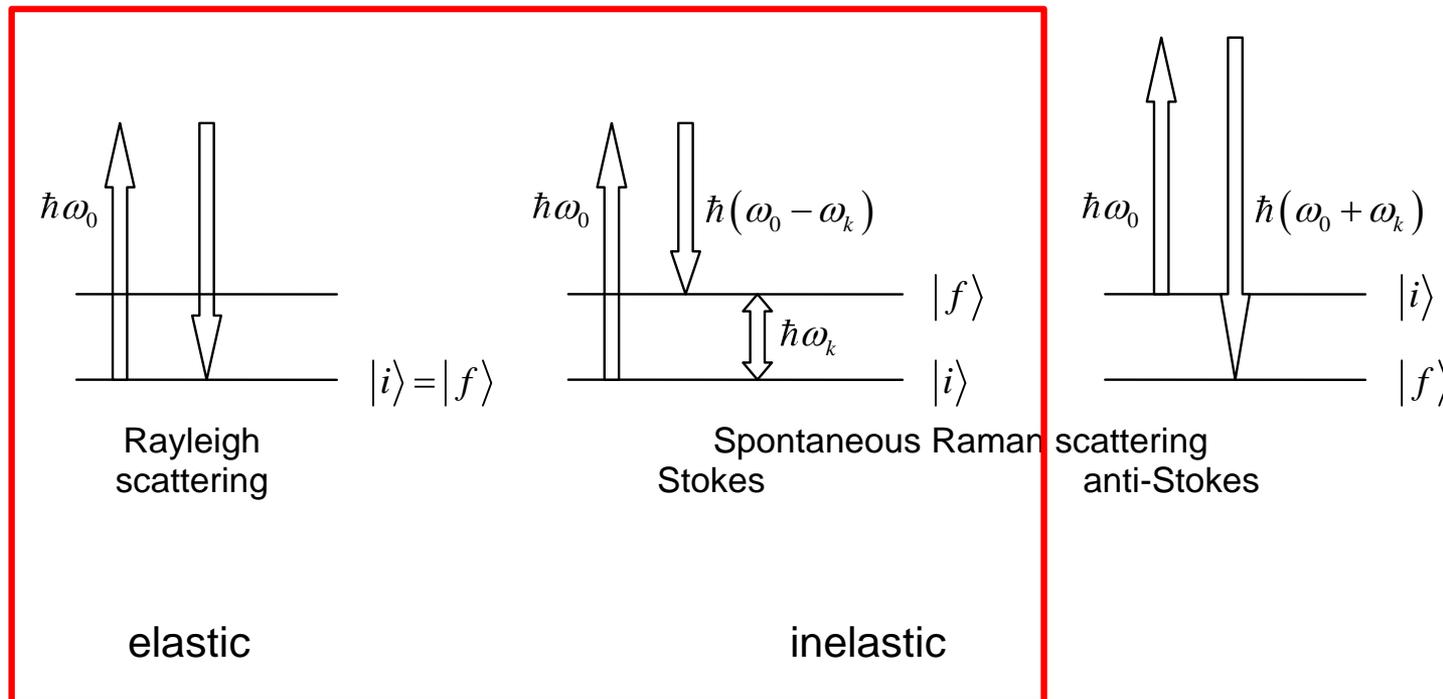


$$\tau_{tot} = \frac{1}{A + P + Q}, \text{ for } P \gg Q: \tau_{tot} = \frac{1}{A + P}$$

Excitation at 248 nm by KrF-Excimer Laser
(A-X) (3-0)-band

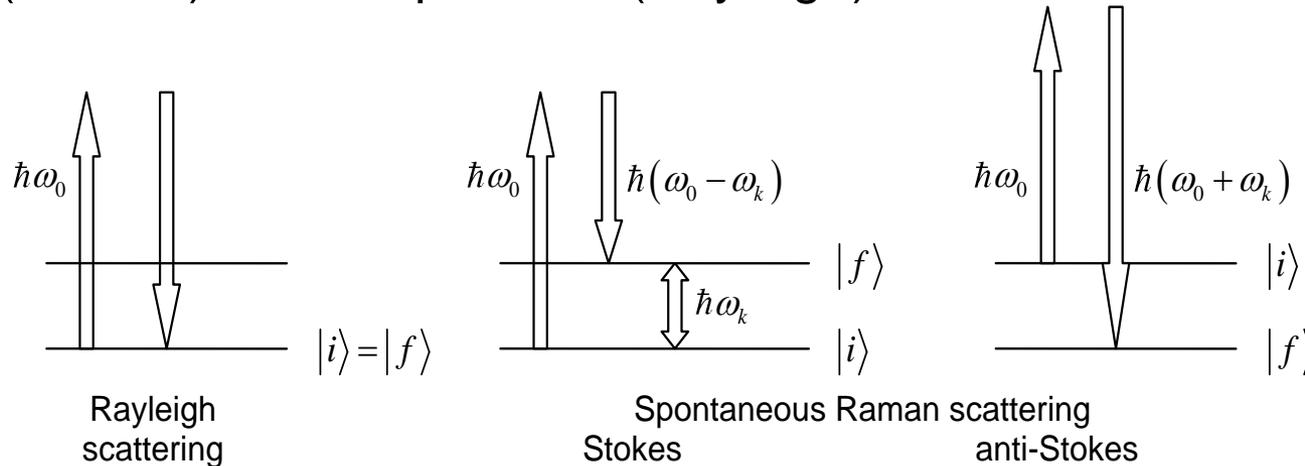
Raman spectroscopy

- Elastic and inelastic light scattering of photons off molecules



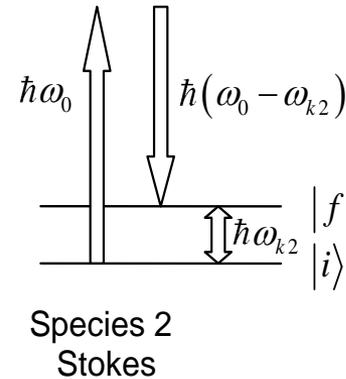
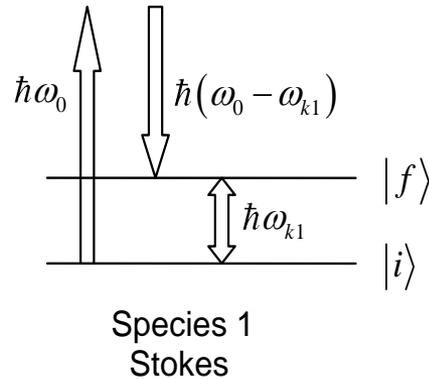
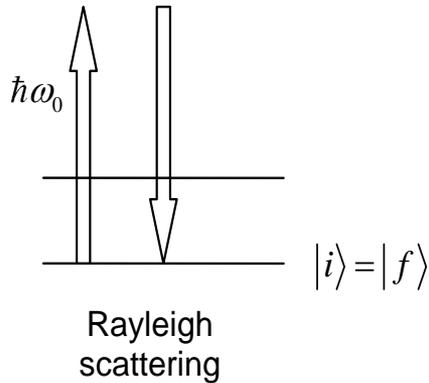
Combined Raman/Rayleigh spectroscopy

- Multi-scalar method: instantaneous measurement of main species (Raman) and temperature (Rayleigh)



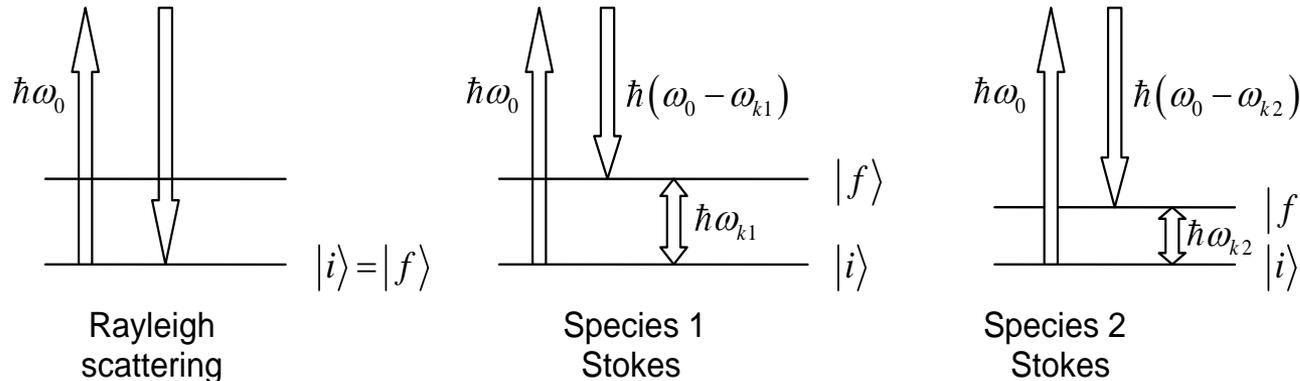
Combined Raman/Rayleigh spectroscopy

- Multi-scalar method: instantaneous measurement of main species (Raman) and temperature (Rayleigh)



Combined Raman/Rayleigh spectroscopy

- Multi-scalar method: instantaneous measurement of main species (Raman) and temperature (Rayleigh)



- Spectral dispersion and simultaneous meas. of: CO_2 , O_2 , CO , N_2 , CH_4 , H_2O , H_2 , equivalence ratio (ϕ), Temp.
- **Challenges:**
 - Low Raman scattering cross-sections and single-shot requirement
 - Data evaluation of noisy data
 - 1D application, high spatial resolution

Raman spectroscopy: selection rules and spectra

- Selection rules

$$\Delta J = 0, \pm 2$$

$$\Delta J = 0 \rightarrow \text{Q-branch}$$

$$\Delta J = +2 \rightarrow \text{O-branch}$$

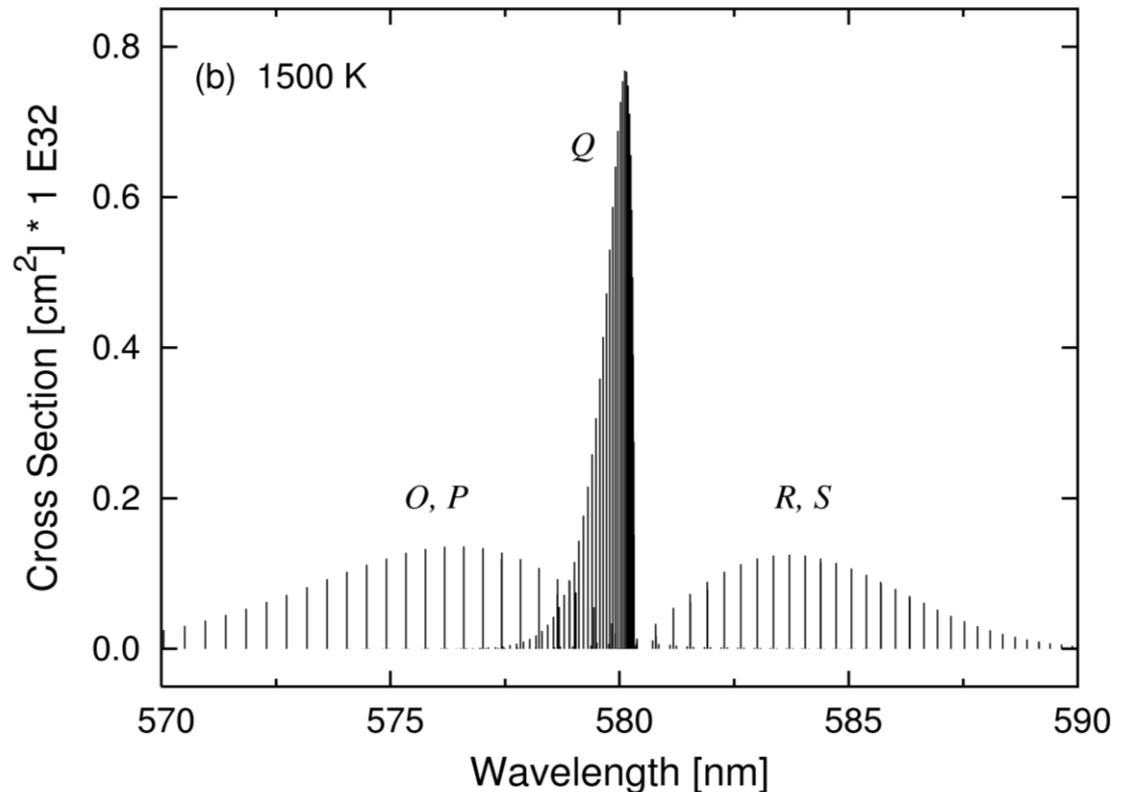
$$\Delta J = -2 \rightarrow \text{S-branch}$$

Oxygen molecule O_2 , $T = 1500 \text{ K}$

Simulated “stick spectrum” – infinite resolution

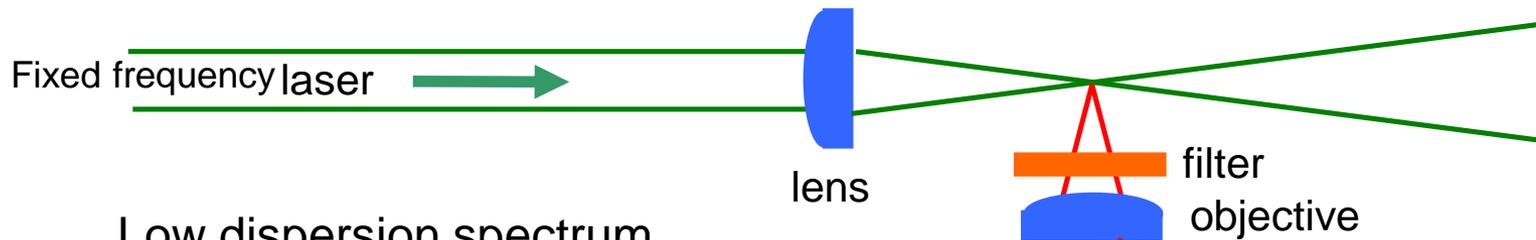
Ro-vibronic Stokes Raman

Exception: very weak R and P-lines

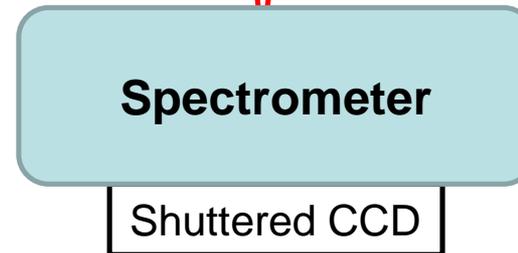
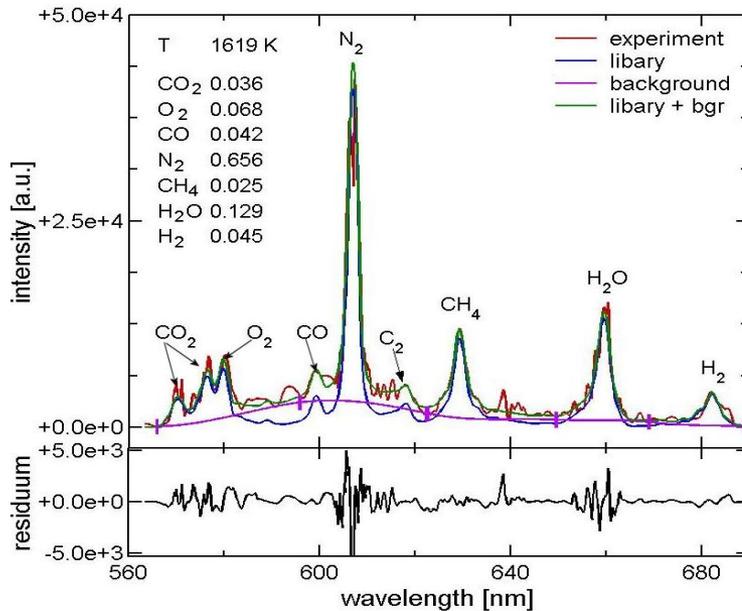


Raman spectroscopy: setup

- Experimental setup

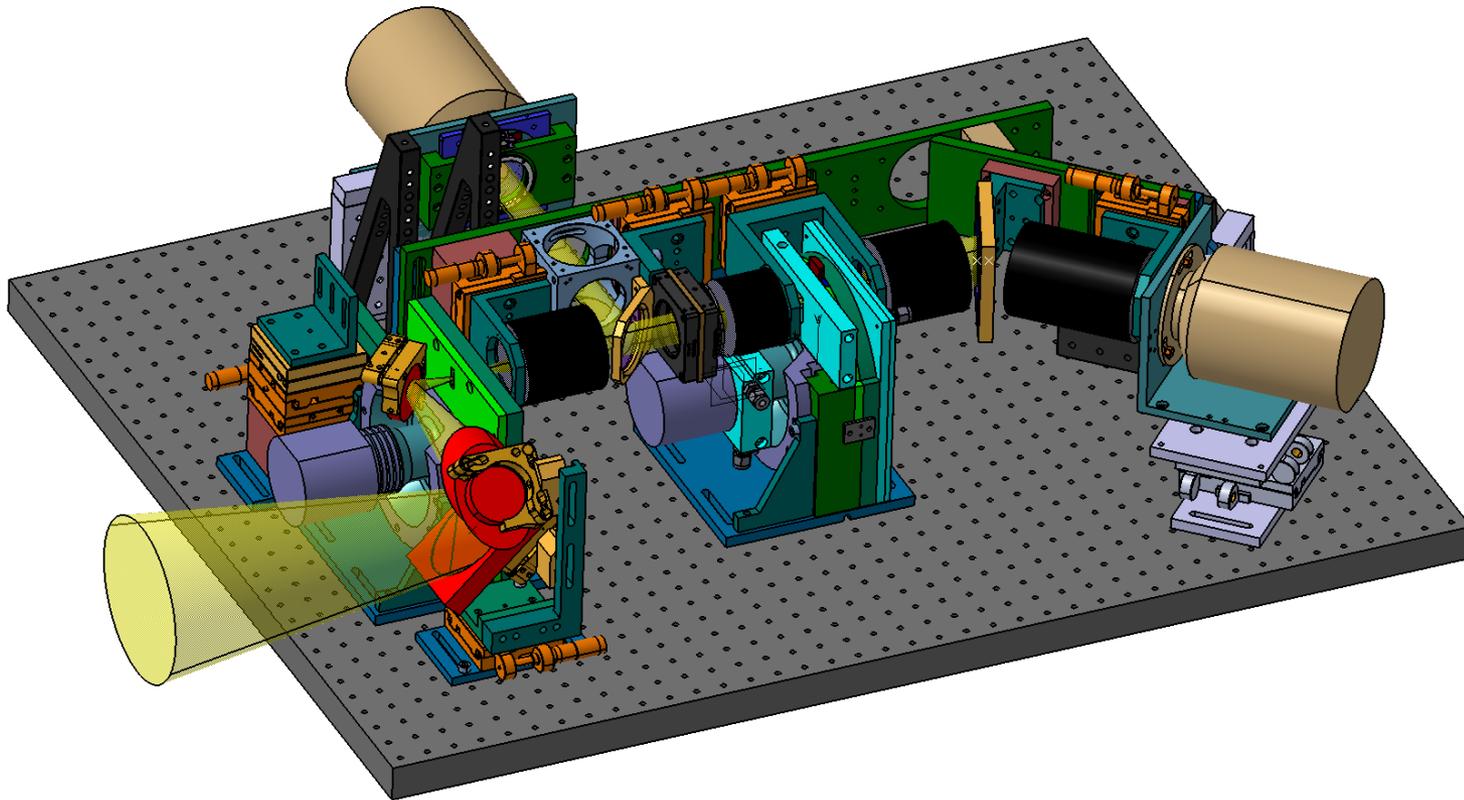


Low dispersion spectrum



1D Raman/Rayleigh: spectrometer

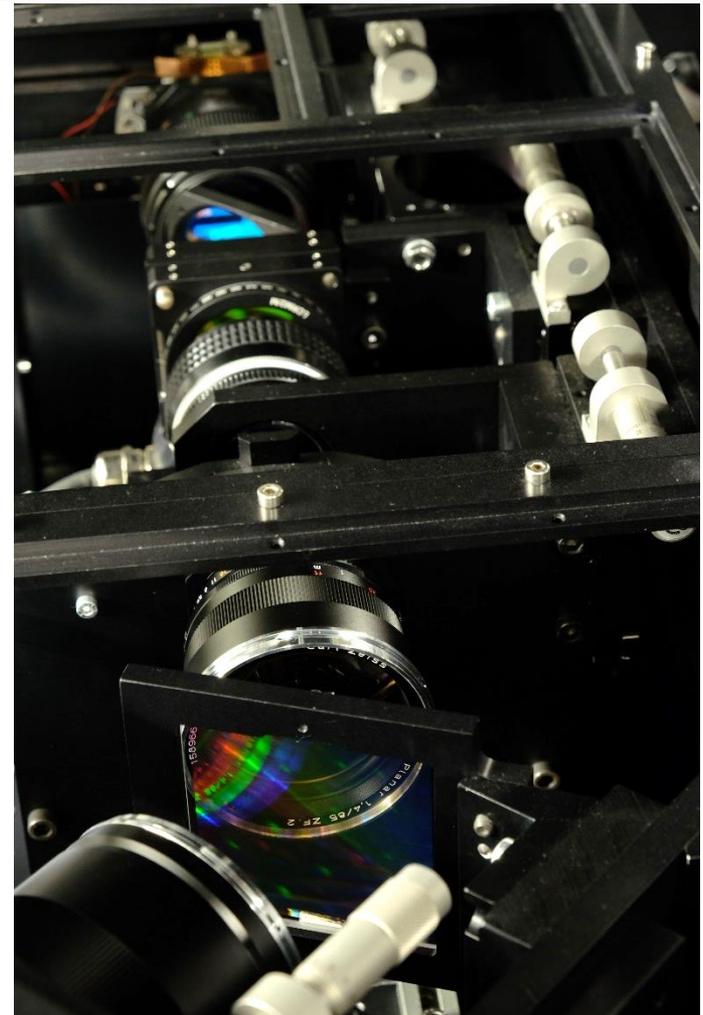
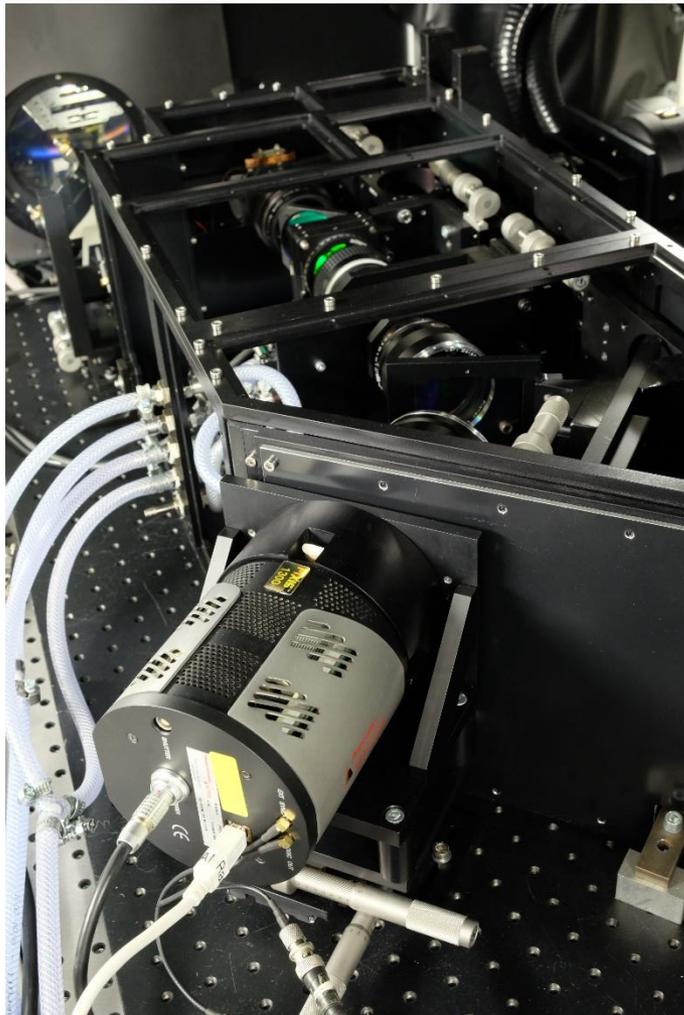
- New TU Darmstadt design



1D Raman/Rayleigh: spectrometer



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1D Raman/Rayleigh spectroscopy: iterative post-processing procedure



- Raman (inelastic) scattering \rightarrow concentrations $N_i(\vec{r})$

$$S_{ram,i}(\vec{r}) \propto \sigma_{ram,i}(T(\vec{r})) I_{Laser} N_i(\vec{r})$$

- Rayleigh (elastic) scattering \rightarrow temperature $T(\vec{r})$

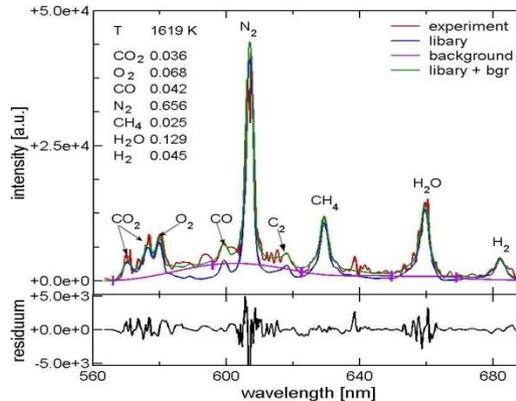
$$S_{ray}(\vec{r}) \propto \sigma_{ray}(N_i(\vec{r})) I_{Laser} \sum N_i(\vec{r})$$

$$\sigma_{ray} = \sum_i \left(\frac{N_i(\vec{r})}{\sum_j N_j(\vec{r})} \right) \sigma_{ray,i} \xrightarrow{\text{Ideal gas law}} T(\vec{r}) \propto \frac{1}{\sum N_i(\vec{r})}$$

- \rightarrow **Determination of N_i , T by iterative procedure:
Need $\sigma_{ram,i}$ of each species i**

Different options for data evaluation

- Spectral fit



- Matrix inversion (MI) method

$$\vec{S} = \underline{\underline{M}} \vec{N}$$

$$\Rightarrow \vec{N} = \underline{\underline{M}}^{-1} \vec{S}$$

Combining the strength of both
→ **The Hybrid MI-method**

A Hybrid Method for Data Evaluation in 1D Raman Spectroscopy

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Motivation

- Spontaneous Raman scattering
 - important technique in combustion research
 - major species, scalar gradients, scalar dissipation
 - need best possible accuracy, precision, and spatial resolution
 - improvements in detection hardware and methods of analysis
- Two approaches to data analysis for hydrocarbon flames; both are complicated
- “Hybrid” method of Raman data analysis
 - combine strengths of methods used by Sandia and TU Darmstadt
 - reduce level of expertise needed to interpret Raman data
- Demonstrate using laminar flame measurements from Sandia system
 - Premixed CH_4 /air flat flames
 - Laminar H_2 jet flame (no hc fluorescence interference)

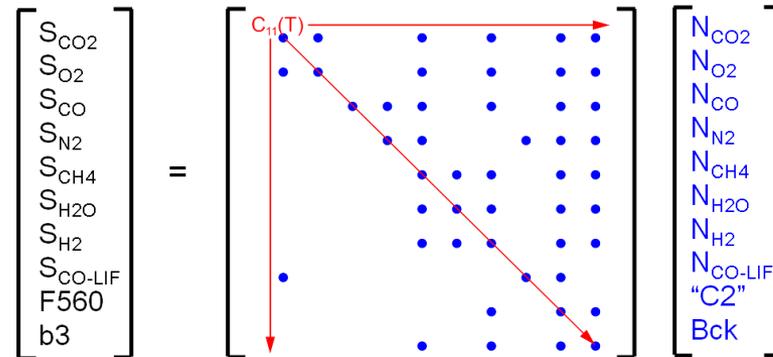


Matrix Inversion (Sandia)

- On-chip binning of Raman bands to reduce camera readout noise
- Matrix equation relating signals and sources

$$S_{CO_2} = C_{1,1}(T) \times N_{CO_2} + C_{1,2}(T) \times N_{O_2} + C_{1,5}(T) \times N_{CH_4} + C_{1,7}(T) \times N_{H_2} + C_{1,9}(T) \times C_2 + C_{1,10}(T) \times Bck$$

Raman
Raman crosstalk
fluorescence
background



- Extensive calibrations to determine temperature dependence of matrix elements for Raman response and crosstalk (represented as polynomials)
- Solve inverse problem to get species concentrations and temperature
- Iterate on Rayleigh temperature (1K conversion, 3-4 iterations)

Spectral Fitting (TU Darmstadt)

- Individual rovibrational Raman transitions calculated for each species, based on Placzek's theory of polarizability (TUD Ramses code)
- Each Raman transition convolved with experimentally determined apparatus function, then all convolved Raman transitions superposed
 - Rayleigh scattering image → apparatus function in this work
 - Raman bands broaden with increasing temperature due to the population of higher quantum states
 - Spectral library composed of temperature-dependent Raman bands
- The spectral library for each molecule is calibrated to an experimental spectrum measured in a gas sample with known mole fraction and temperature.
- Details of fitting procedure (Dirk Geyer thesis)

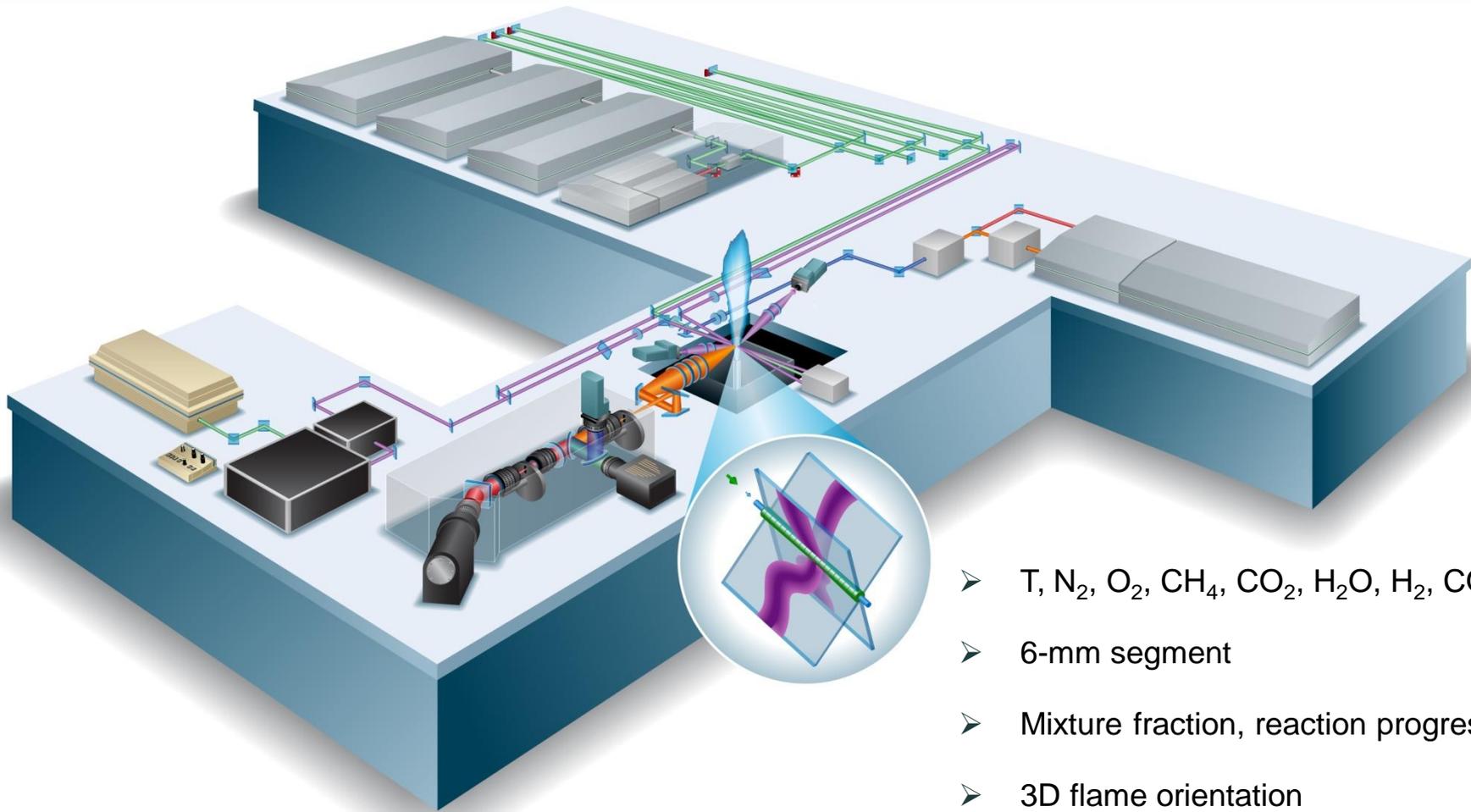
Matrix Inversion (old version)

- Pro's
 - Lower noise
 - Faster acquisition & processing
- Con's
 - Extensive calibrations required
 - Cannot calibrate accurately at some conditions
 - Spectral information lost
 - Impractical to account for beam steering or spatial dependence of response function

Spectral Fitting

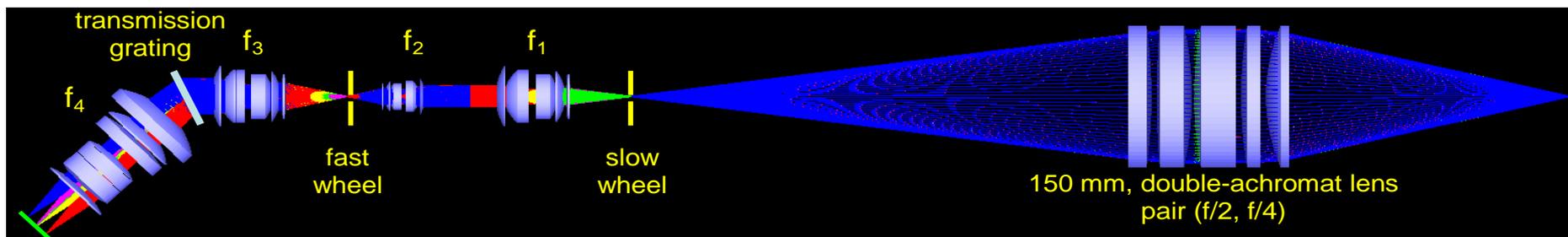
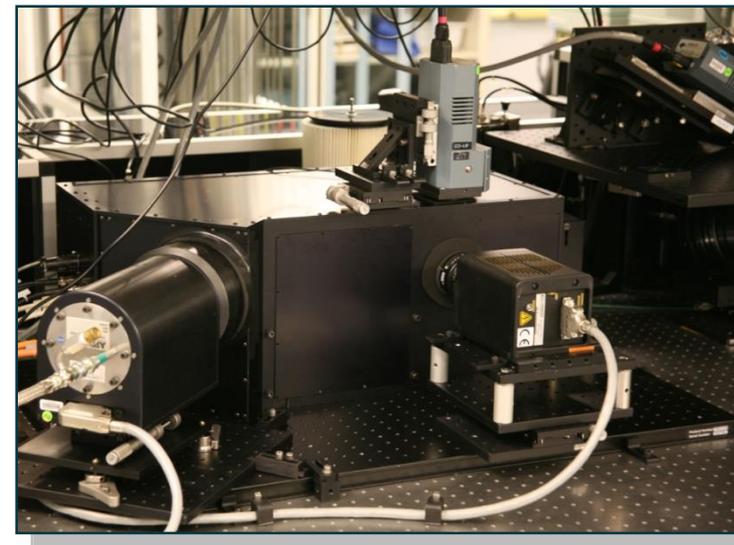
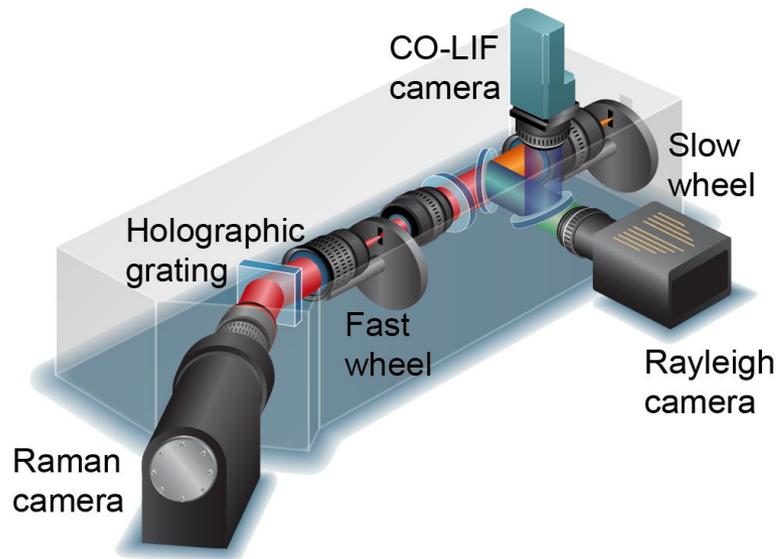
- Pro's
 - Based on quantum mechanical theory
 - One calibration per species
 - Beam steering handle automatically
 - Background corrected more rigorous
- Con's
 - Higher readout noise
 - Slower data acquisition rate
 - Significant time/effort in fitting

Turbulent Combustion Laboratory: Raman/Rayleigh/CO-LIF & Crossed OH PLIF



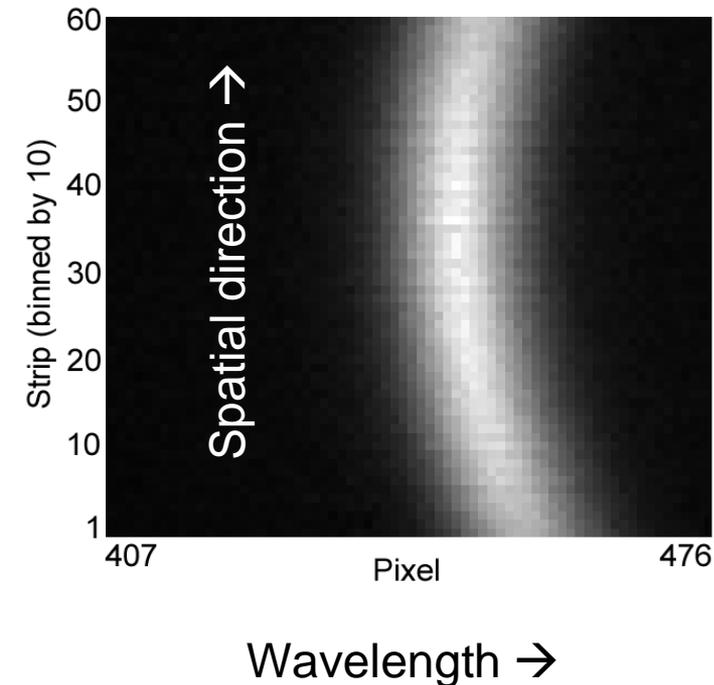
- T, N₂, O₂, CH₄, CO₂, H₂O, H₂, CO
- 6-mm segment
- Mixture fraction, reaction progress
- 3D flame orientation
- 1D, 3D scalar gradients, dissipation

Detection System



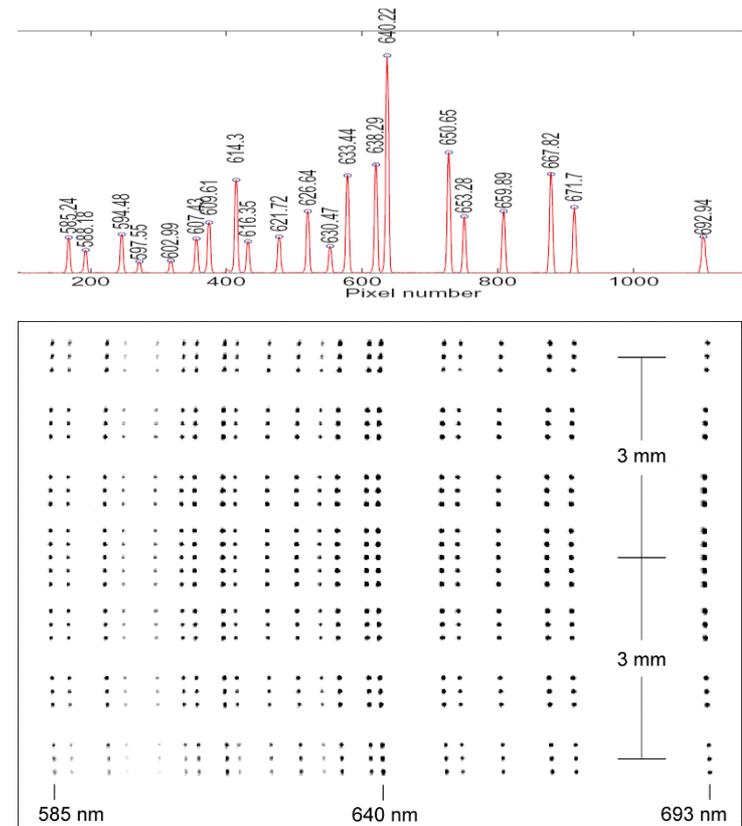
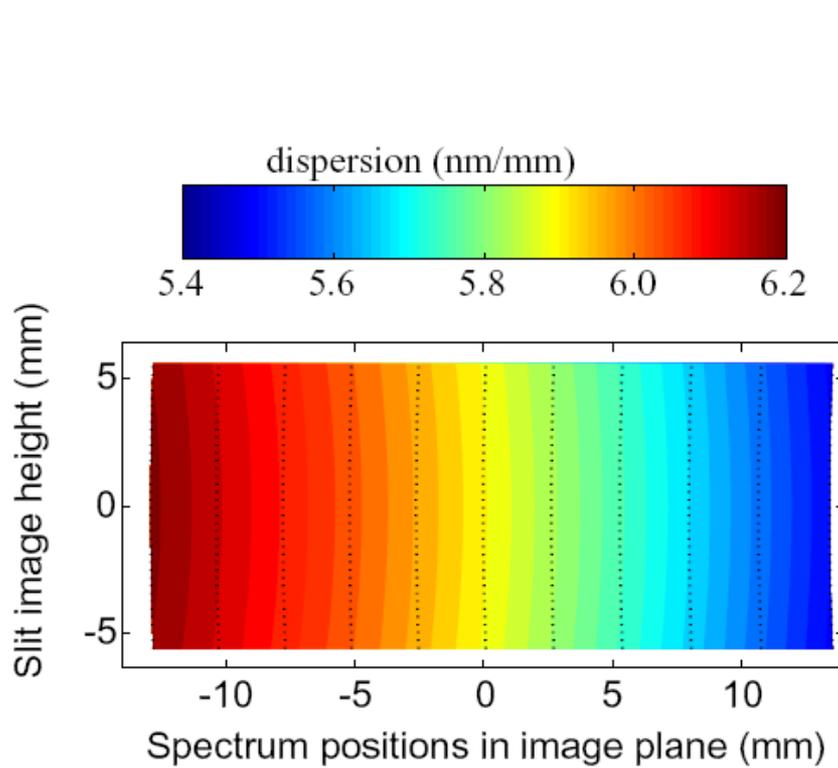
- LSF 40-60 μm
- Mechanical gate: 3.9 μs gate (FWHM)
- Transmission grating
- 103 μm data spacing

Optical Bowing Effect



- Image of N₂ Raman scattering in air
- Low f-number spectrograph
 - bowed image of slit
 - Jun Zhao, *Appl. Spectr.* 57, 11 (2003) 1368-1375
- Calculated (Zemax) and measured
 - Map CCD for wavelength at each pixel
- Must account for this optical effect

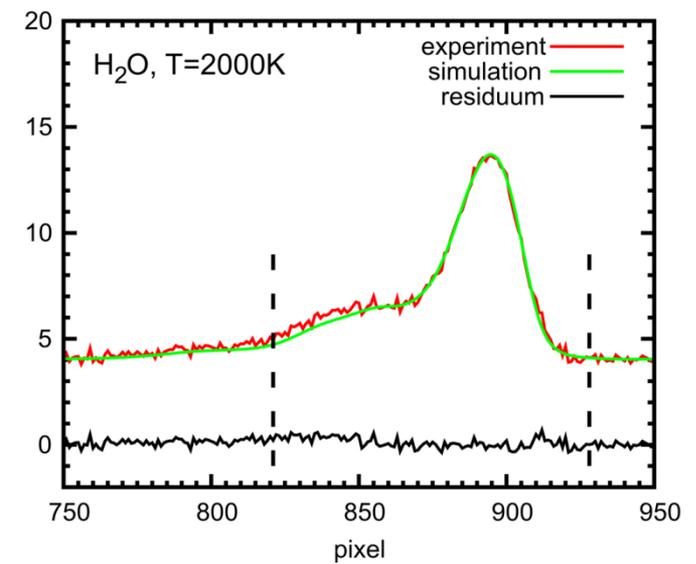
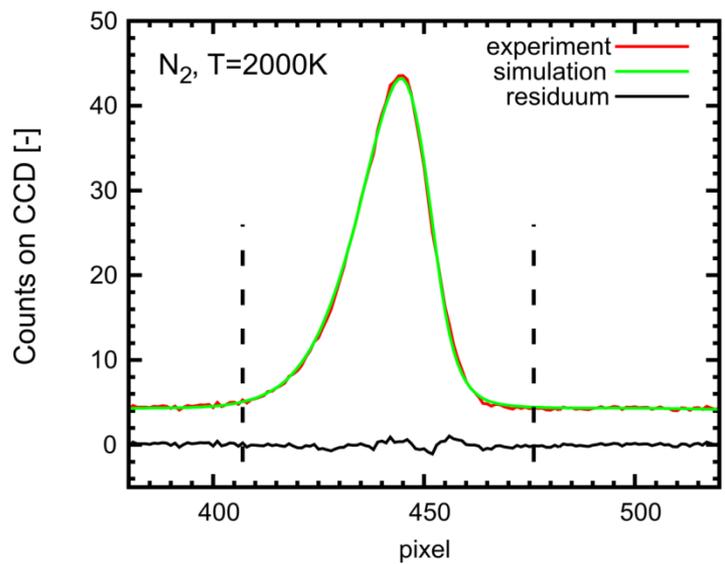
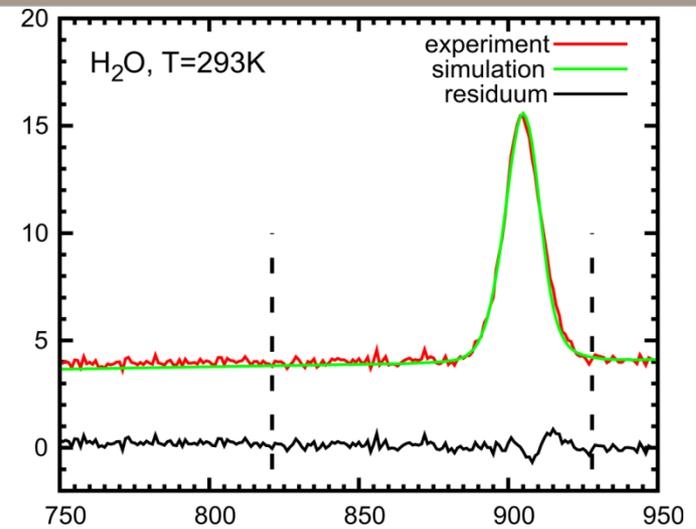
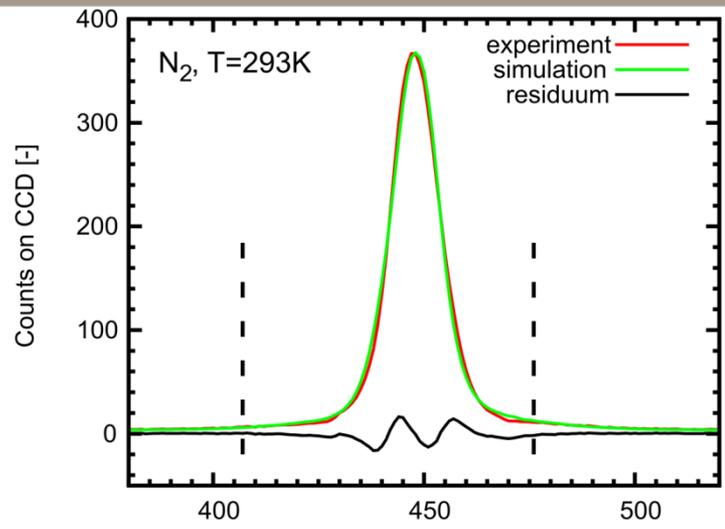
Spectrometer Characteristics



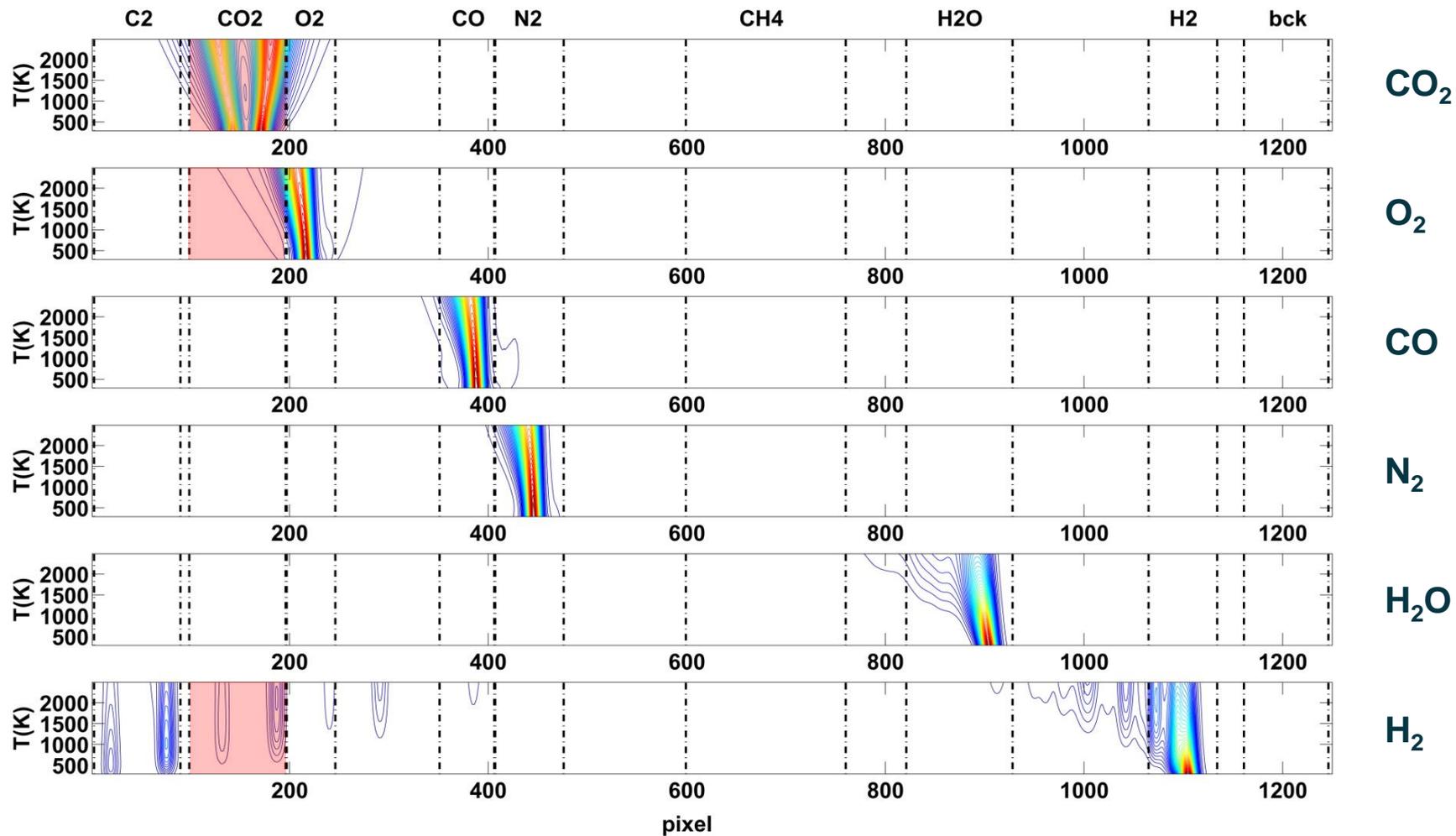
- Calculated (Zemax) dispersion is not linear across the image plane
- Spectral/spatial calibration using neon lamp and target with 50- μm holes on 200- μm centers



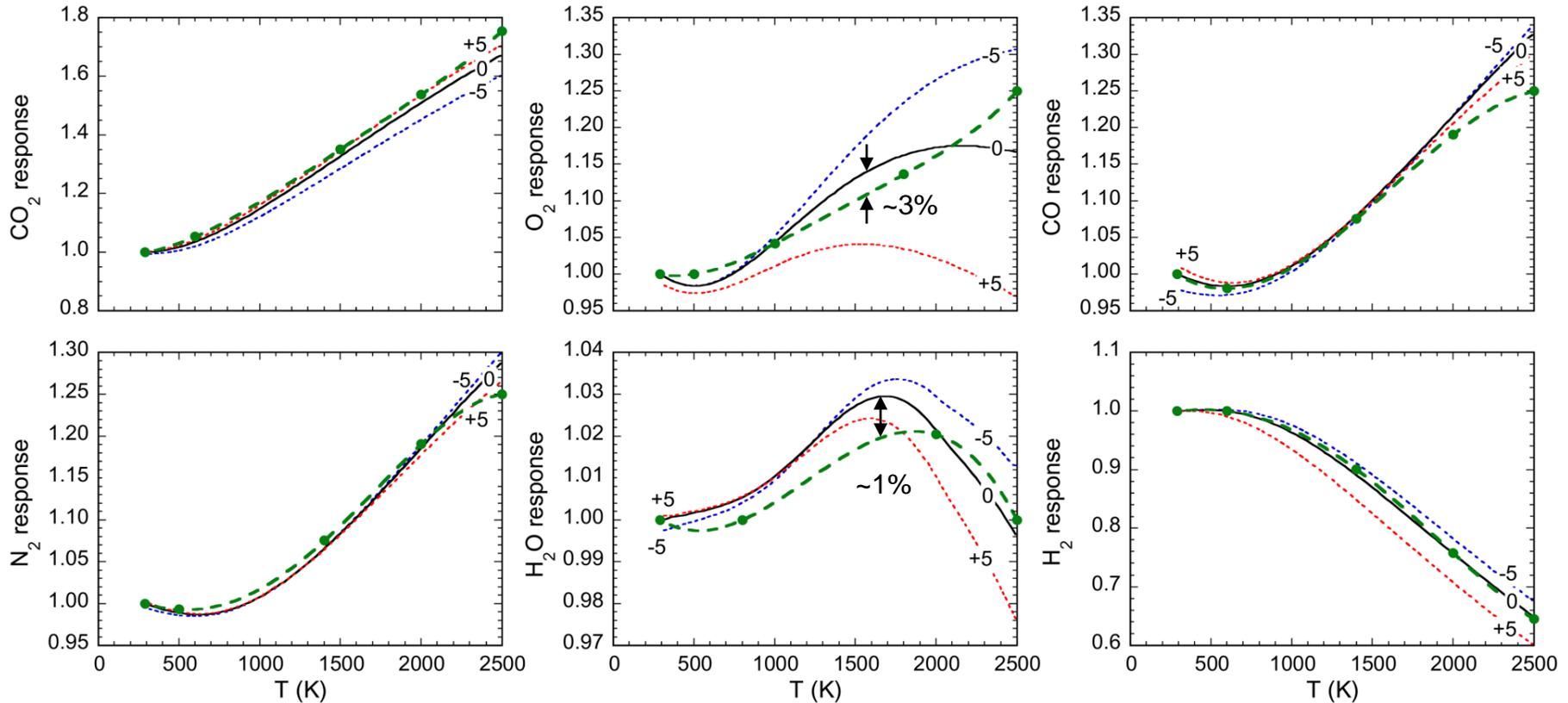
Spectral Library vs. Measurement



Calculated Spectral Libraries (Ramses code)

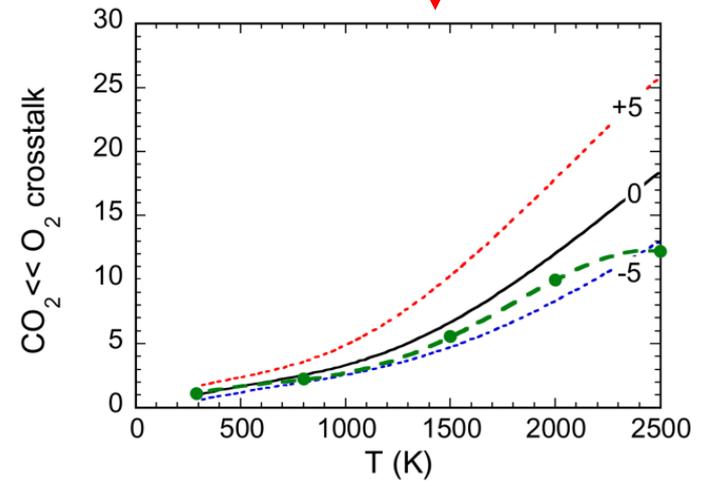
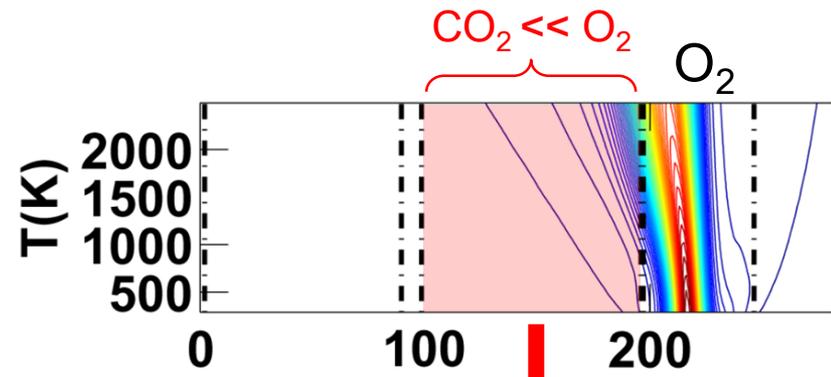
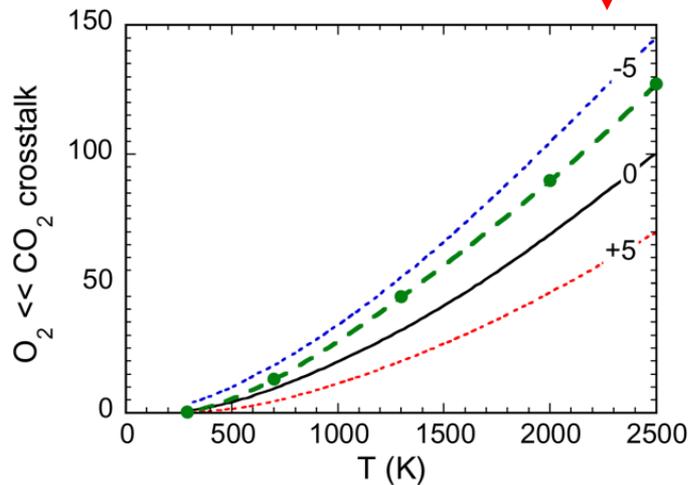
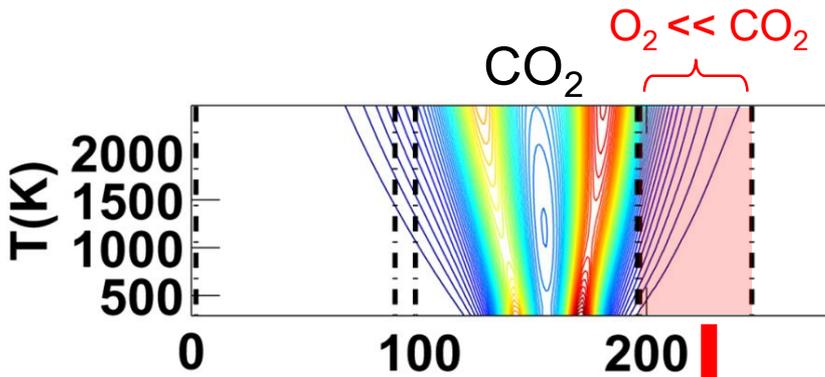


Major Species Response Curves



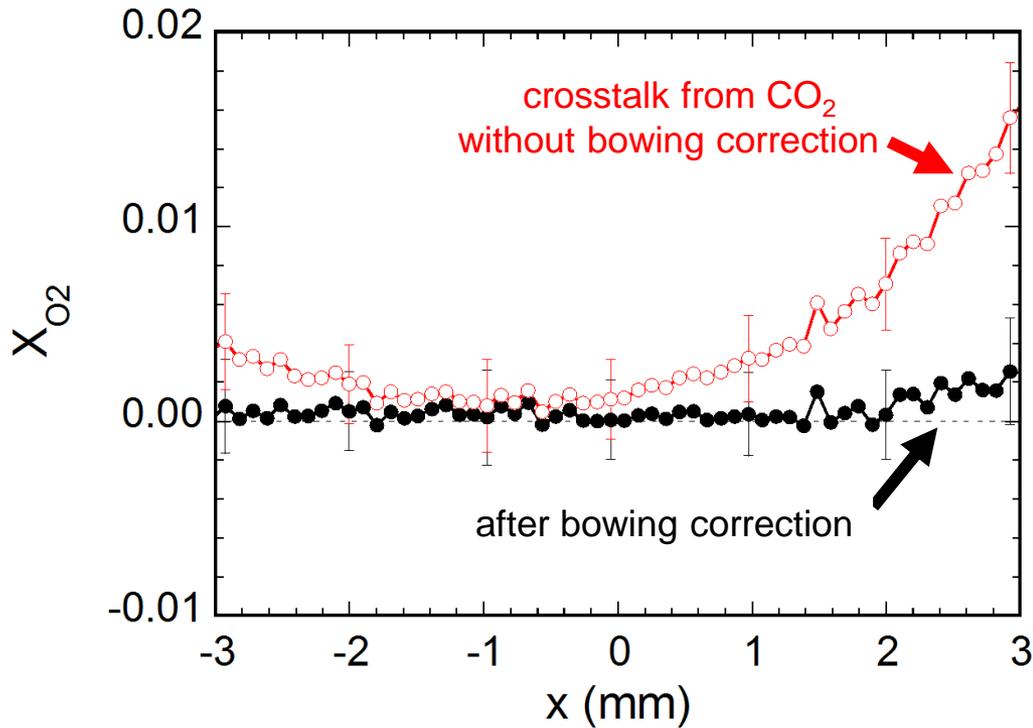
- Good agreement, except for O₂ curve shape at high T
- O₂ response sensitive to bowing effect and beam steering

Crosstalk between CO₂ and O₂



- Greater uncertainty in calibration polynomials
- Sensitive to bowing effect and beam steering

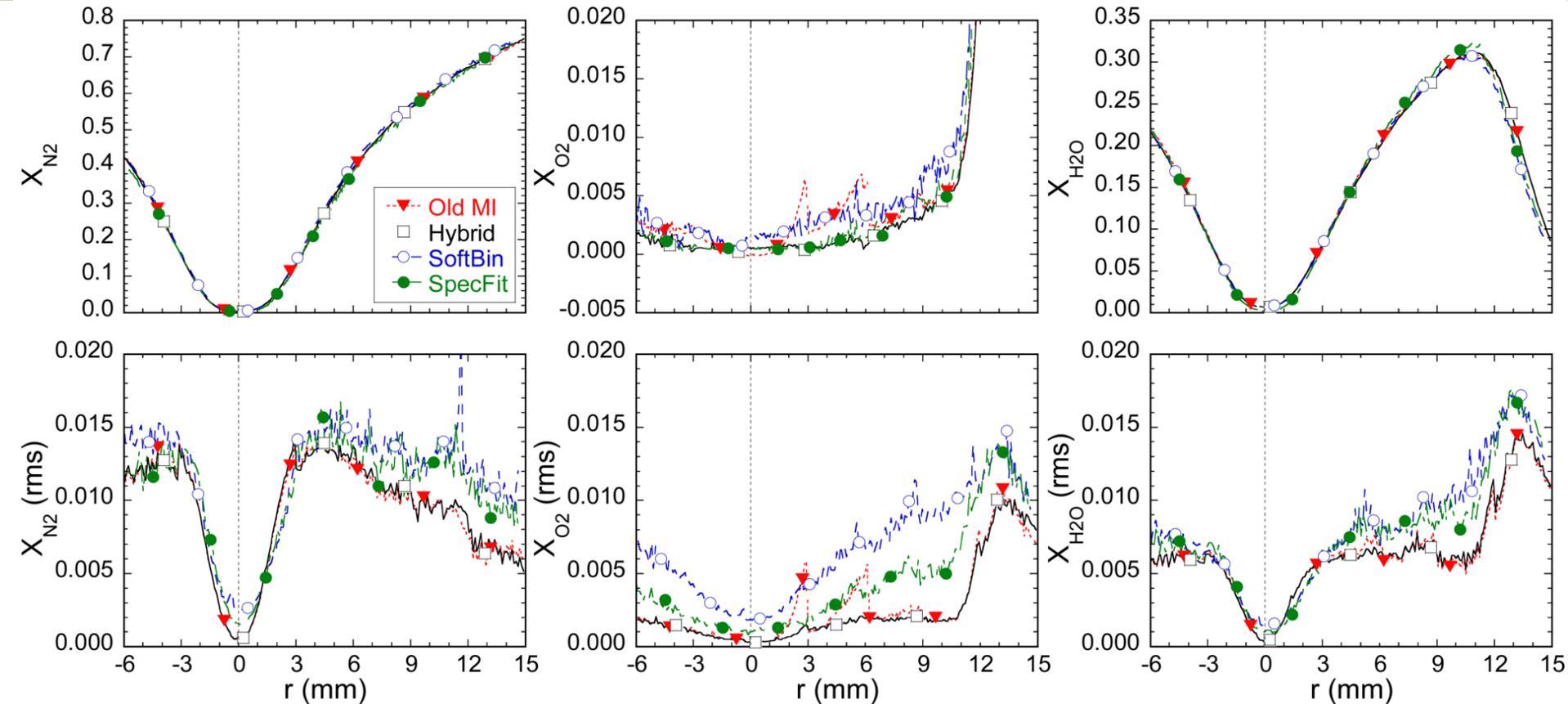
Effects of Image Bowing on O₂ Errors



premixed CH₄/air
"flat" calibration flame

- O₂ mole fraction should be zero in the rich flame products ($\phi=1.3$)
- Bowing effect leads to error of $X_{O_2} \sim 1.6\%$ due to uncorrected CO₂ crosstalk

Comparison for Laminar H₂ Jet Flame



- Close agreement on mean values from hybrid-MI and spectral fitting
- Hybrid method yields better precision (on chip binning)
- Spectral fitting yields lower noise than MI with software binning

Conclusions

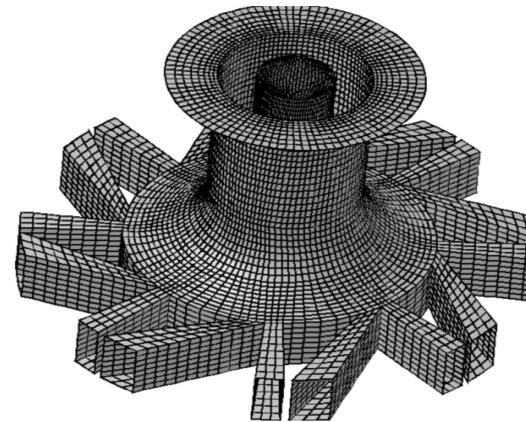
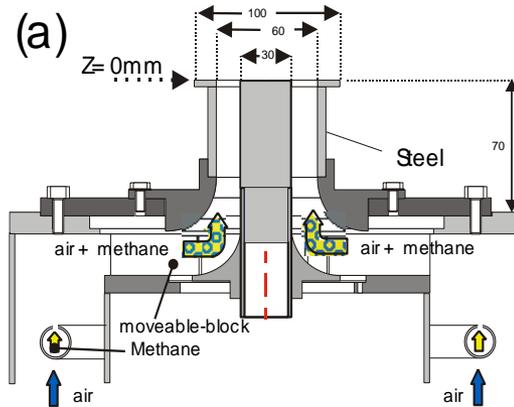
- Hybrid method of Raman data analysis has been developed
 - Calculated Raman libraries are integrated to determine temperature-dependent terms for matrix inversion
 - Response and cross talk for N_2 , O_2 , H_2 , CO , CO_2 , H_2O
- Combines advantages from both previous methods
 - Low noise from on-chip binning
 - Fast data acquisition and processing
 - Temperature dependence based on QM theory
 - Automatic correction for image bowing and beam steering
- Relatively easy to adapt to other Raman/Rayleigh systems

Application example

- Thermo-chemical state in swirling premixed flame:
Gregor et al. Dreizler. Proc. Combust. Inst. 32, 1739 – 1746 (2009)

Thermo-chemical state in swirling premixed flame

- Burner

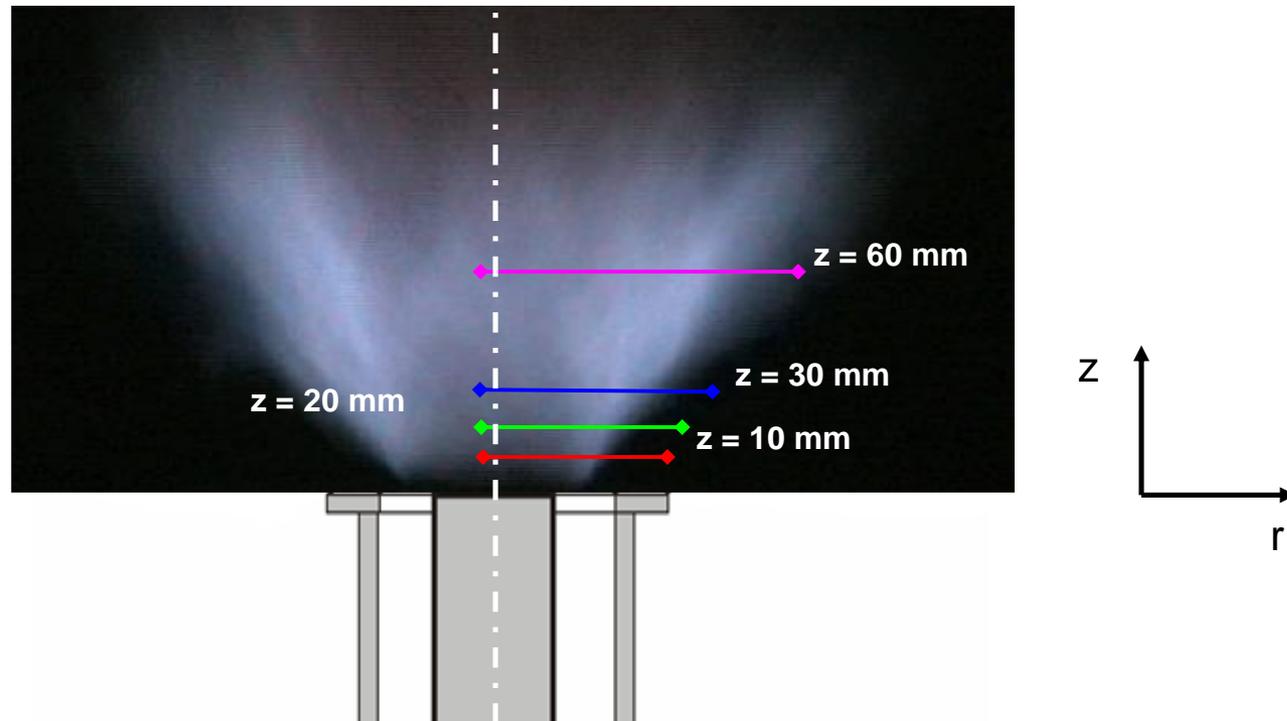


- Operational conditions

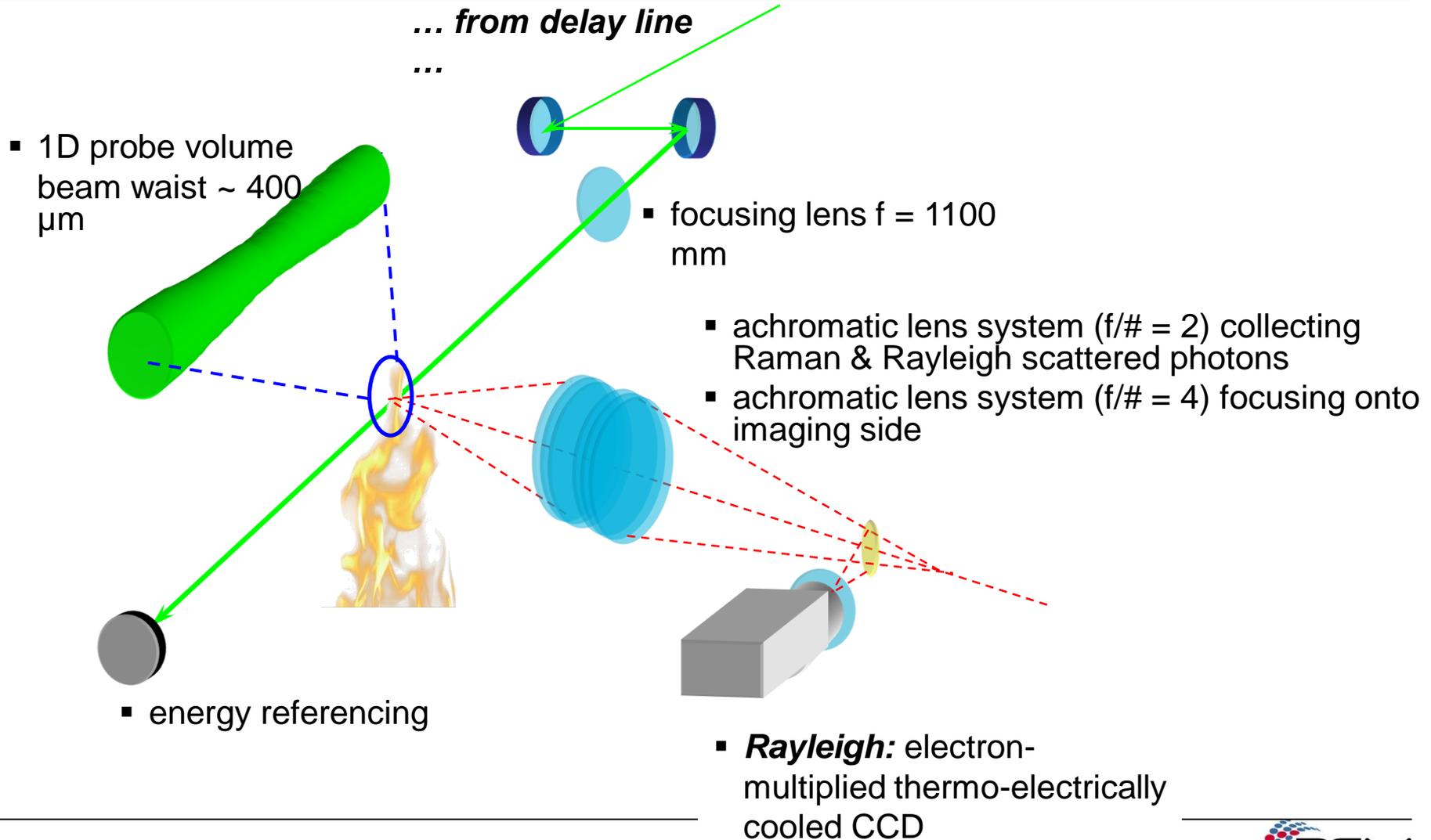
		<i>PSF-30</i>	<i>PSF-90</i>	<i>PSF-150</i>
$S_{0,th}$	[-]	0.75	0.75	0.75
P	[kW]	30	90	150
ϕ	[-]	0.833	0.833	1.0
$Re_{tot.}$	[-]	10000	29900	42300

Measurement locations

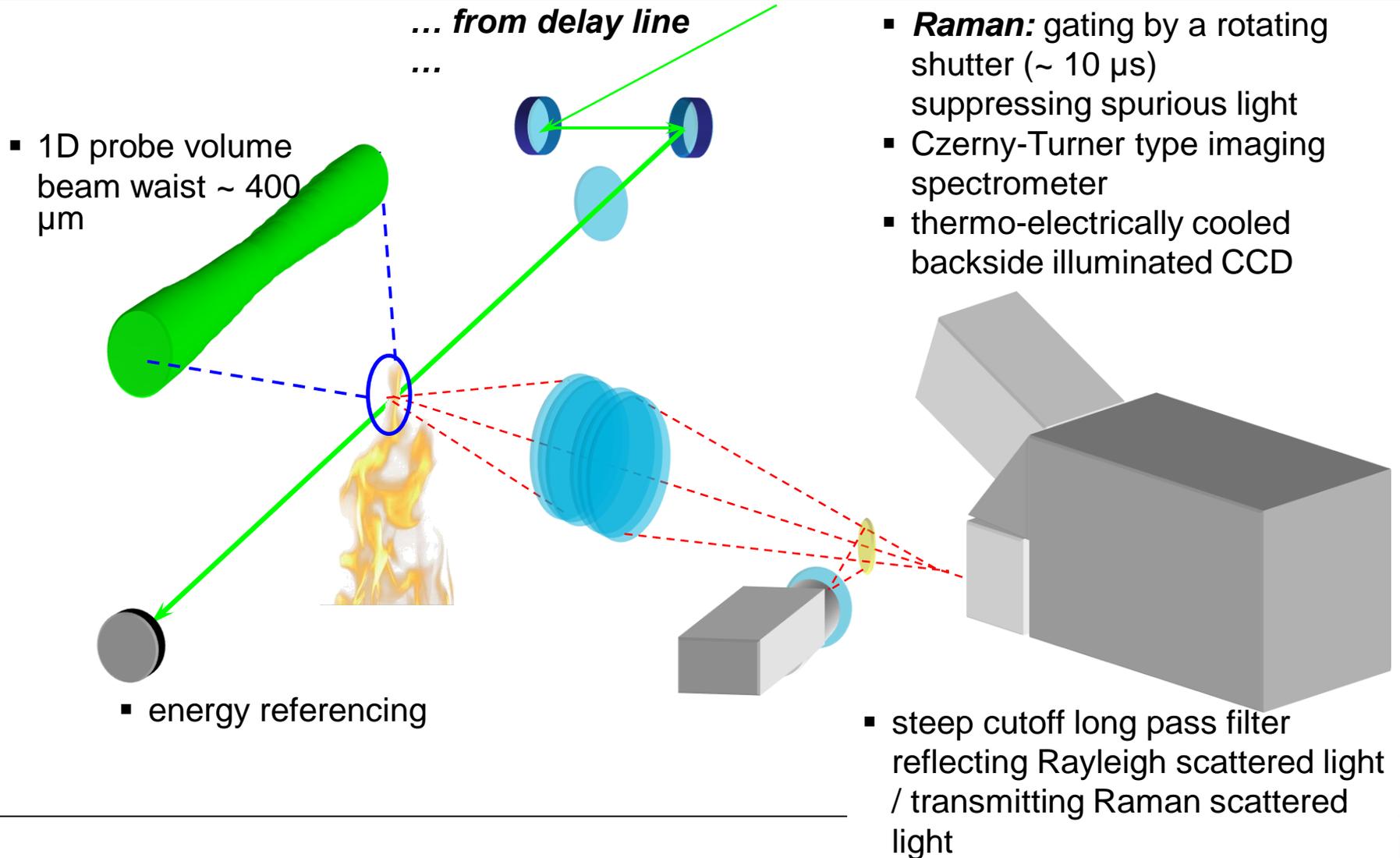
- Radial profiles at 4 axial heights



Raman scattering – exp. setup

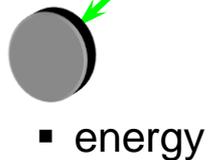
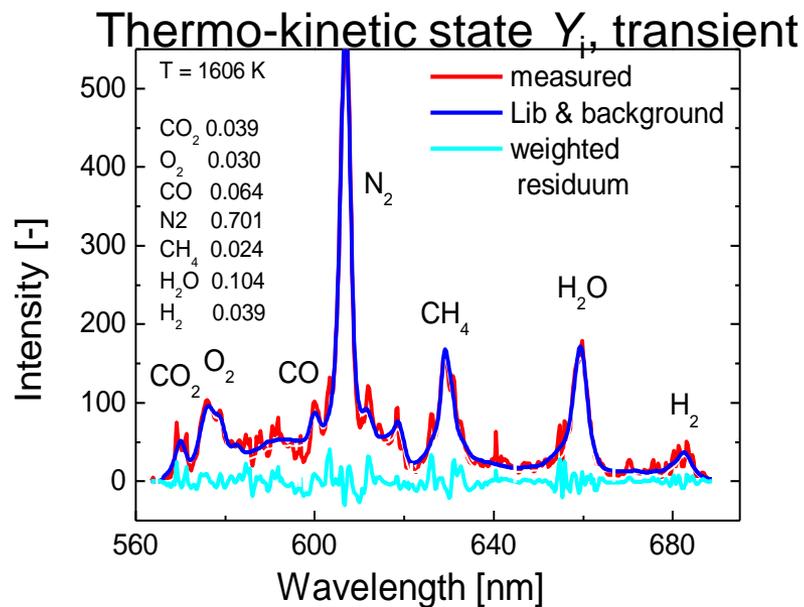


Raman scattering – exp. setup

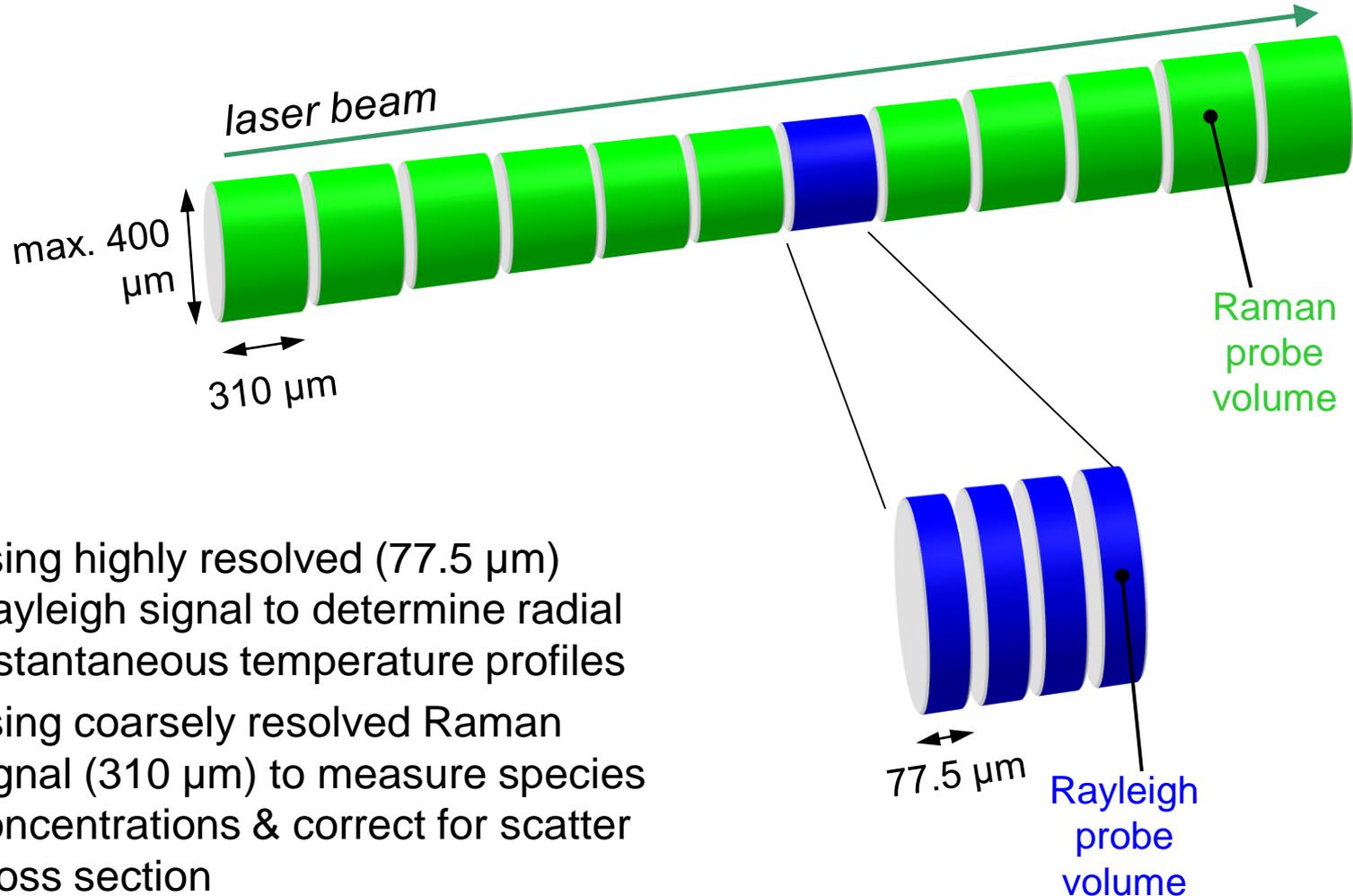


Raman scattering – exp. setup

Data evaluation is conducted with a spectral fitting method using theoretical Raman spectra

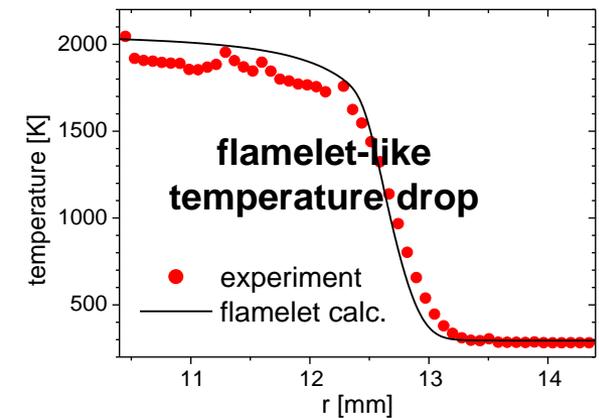
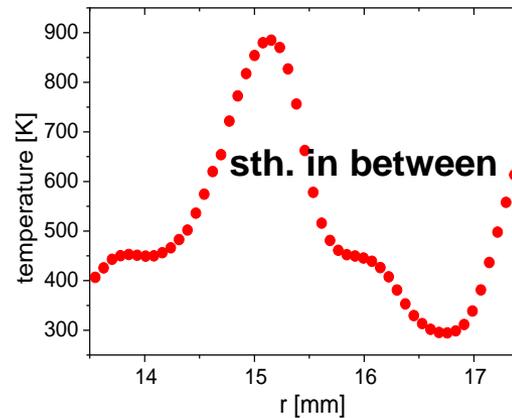
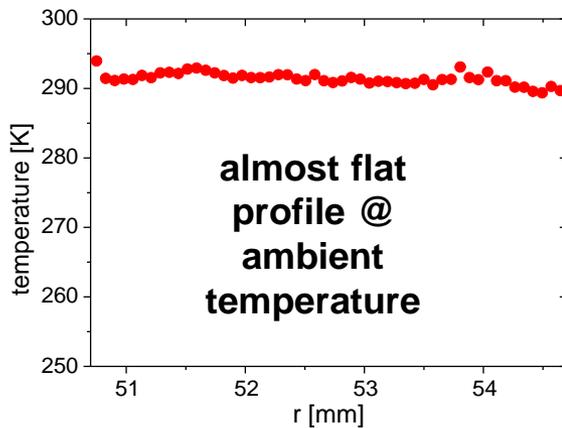
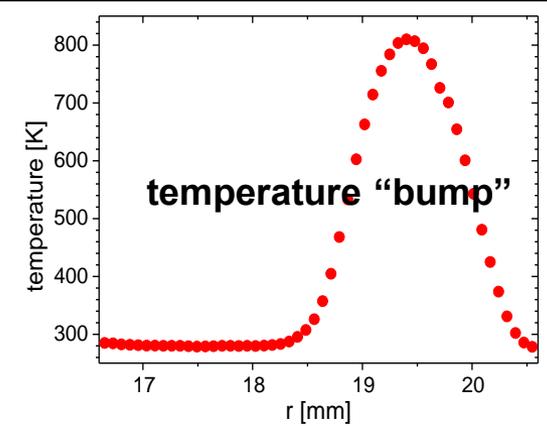
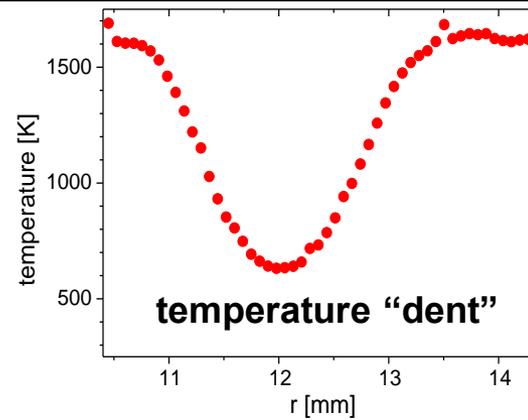
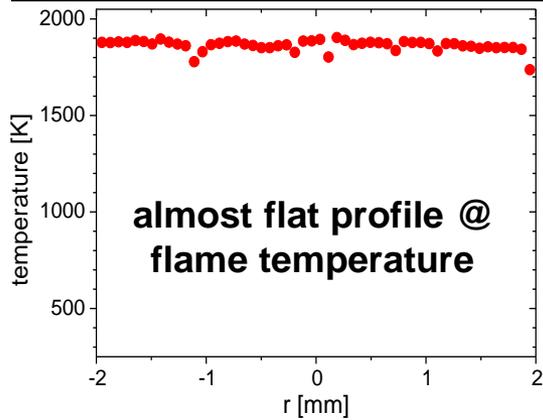


Raman scattering – spatial resolution

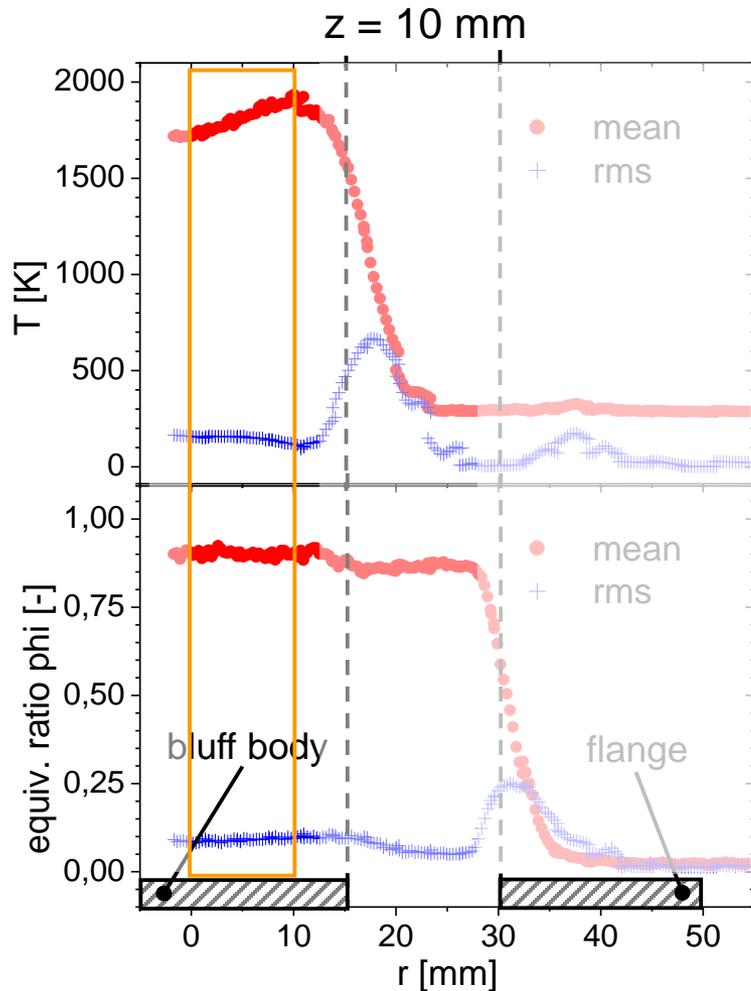


- using highly resolved (77.5 μm) Rayleigh signal to determine radial instantaneous temperature profiles
- using coarsely resolved Raman signal (310 μm) to measure species concentrations & correct for scatter cross section

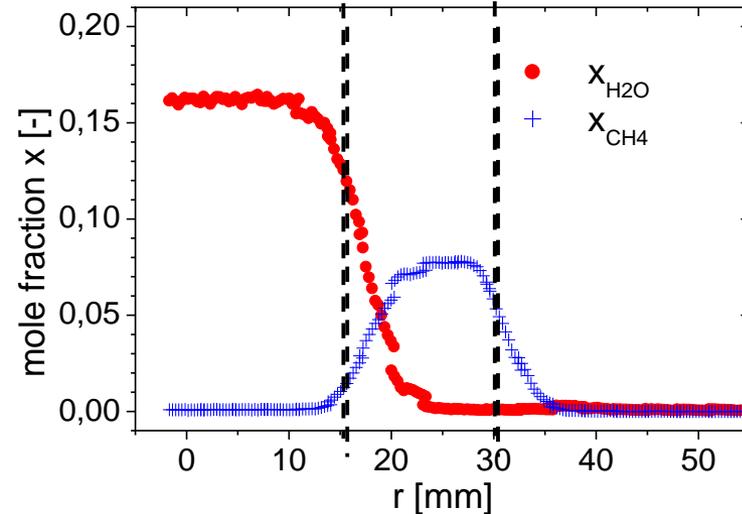
Raman scattering – spatial resolution



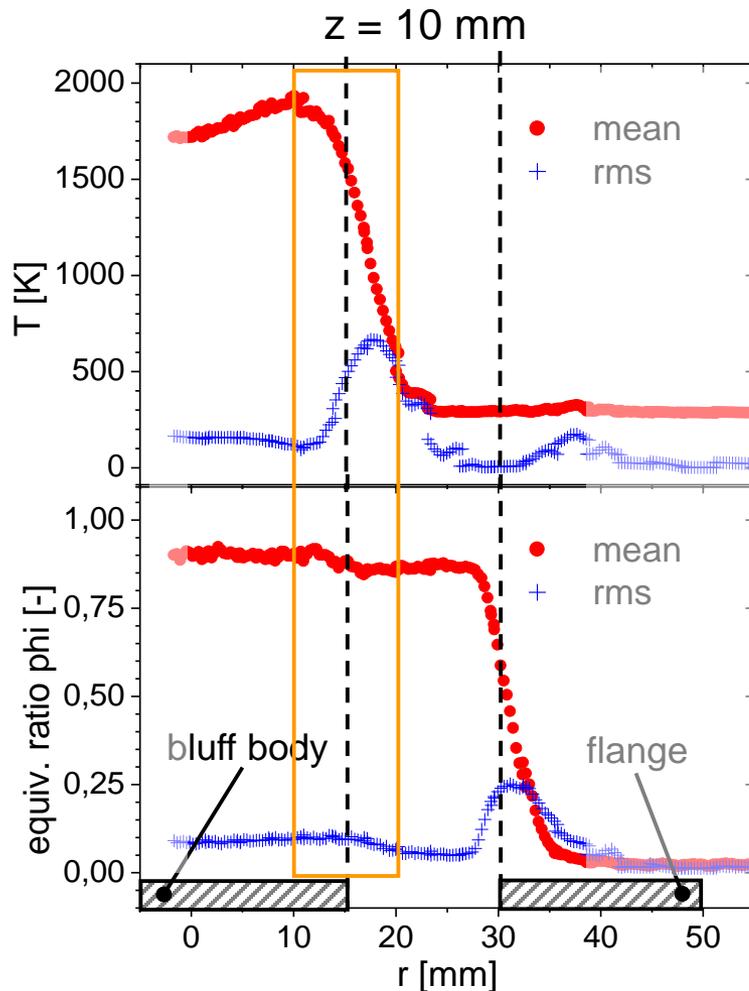
Radial Profiles (mean and rms)



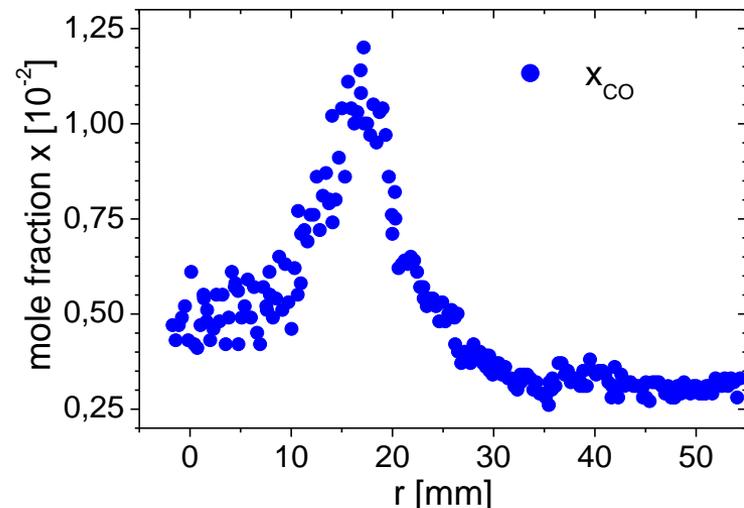
- inner recirculation zone (~0-10mm):
 - fully burnt exhaust
 - heat loss to bluff body



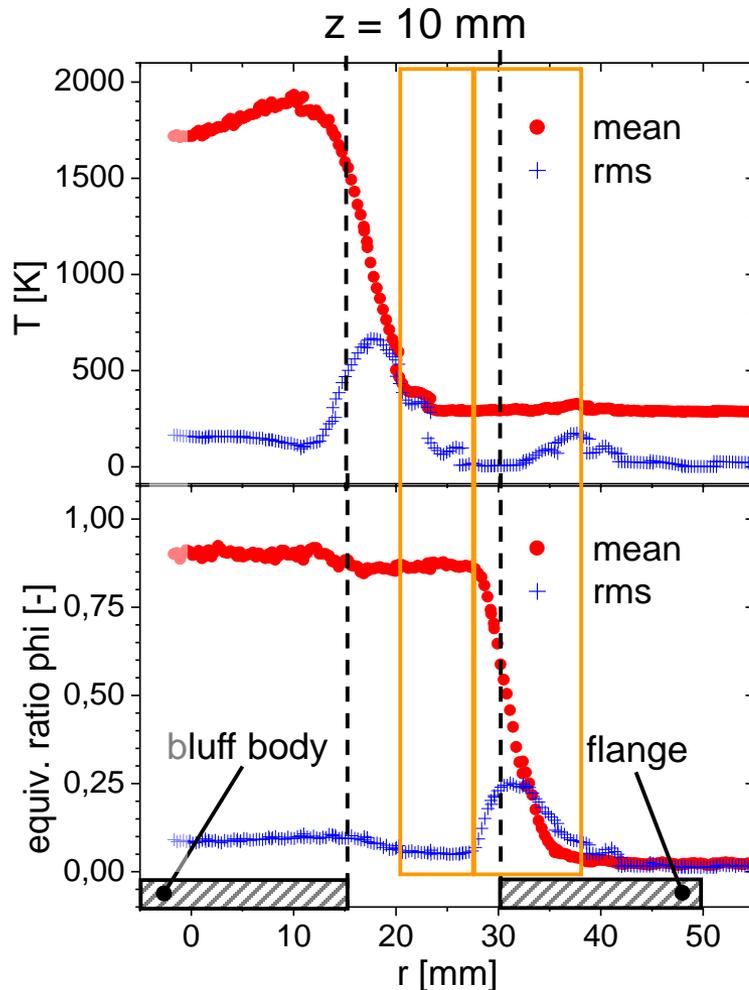
Radial Profiles (mean and rms)



- inner recirculation zone (~0-10mm):
 - fully burnt exhaust
 - heat loss to bluff body
- inner mixing layer (~10-20mm):
 - strong intermittency hence high fluctuation levels
 - $r \sim 17$ mm: mean premixed flame front position as deduced from max. T & c gradients / max. CO concentration

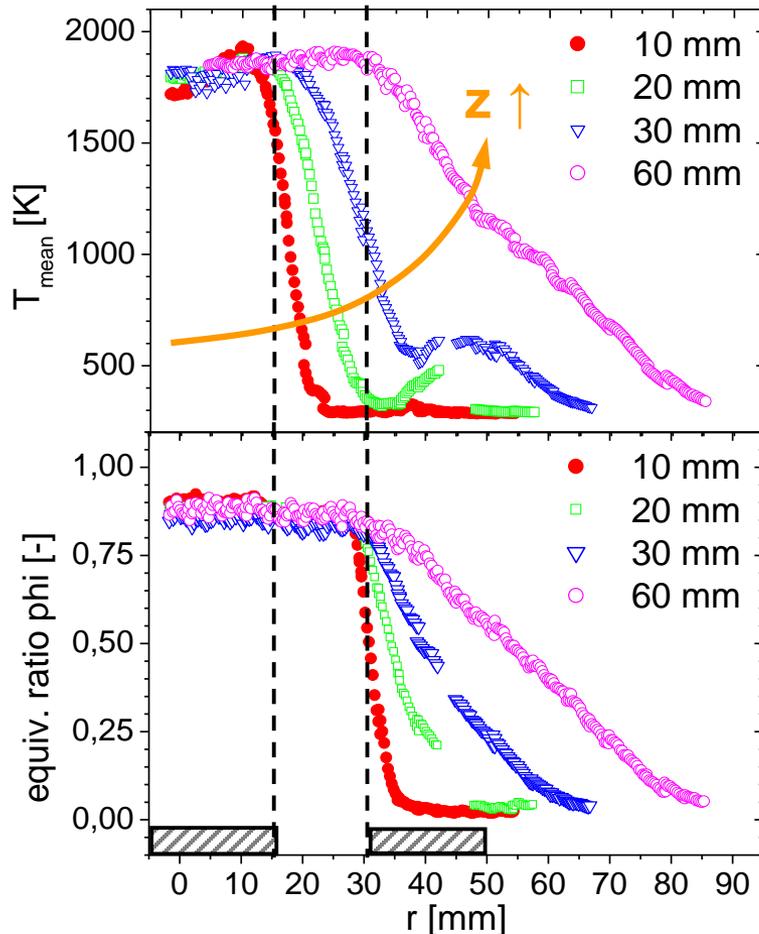


Radial Profiles (mean and rms)



- inner recirculation zone (~0-10mm):
 - fully burnt exhaust
 - heat loss to bluff body
- inner mixing layer (~10-20mm):
 - strong intermittency hence high fluctuation levels
 - $r \sim 17$ mm: mean premixed flame front position as deduced from max. T & c gradients / max. CO concentration
- central annular jet (~20-27mm):
 - almost unreacted fuel without dilution
- outer mixing layer (~27-38mm):
 - steep ϕ gradient towards surrounding air ($\phi = 0$)
 - second temperature maximum due to outer recirculation zone

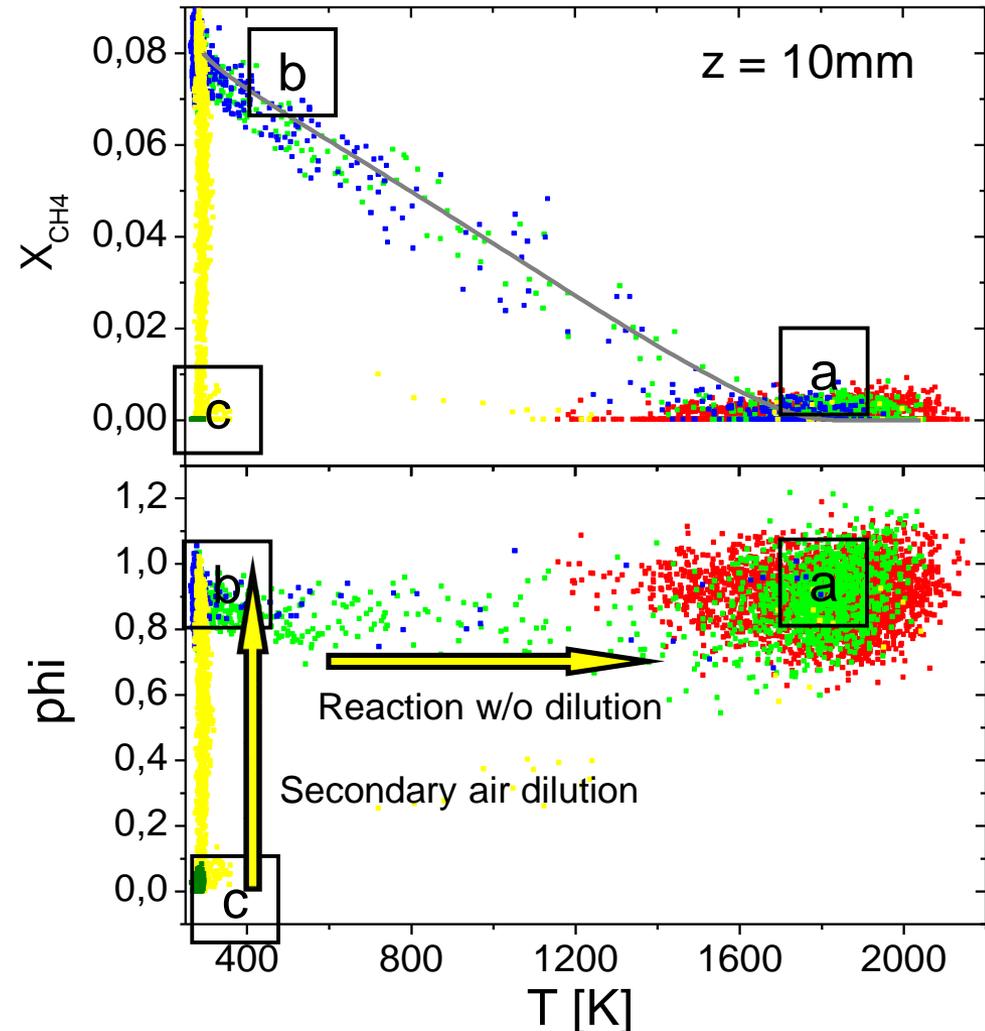
Mean Radial Profiles - z Dependency



- for increasing height z :
 - mean flame front position at larger radii
 - wider flame brush & broader mixing layer hence flatter radial T & ϕ profiles
 - distinct 2nd T maximum (up to $z = 30$ mm) due to outer recirculation of exhaust
 - premixed flame front is located in regions with very low stratification of nearly constant ϕ (up to $z = 30$ mm)

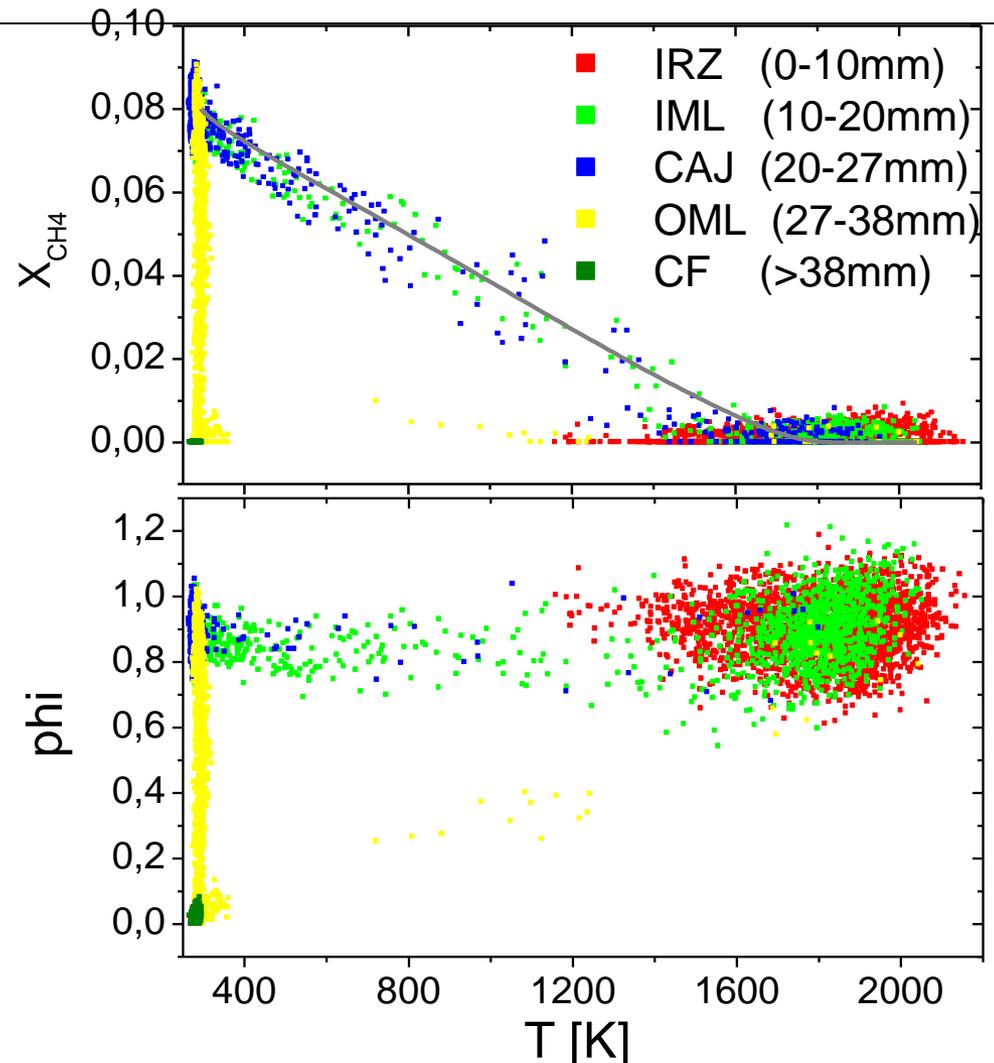
Single Shot Correlations - Scatter Plots

- single shot correlation between 2 or more scalars (e.g. T & CH₄)
- each scatter corresponds to one single shot
- samples spanned between 3 thermo-kinetic states:
 - a) hot burnt exhaust
 - b) cold unburnt fuel
 - c) cold secondary air



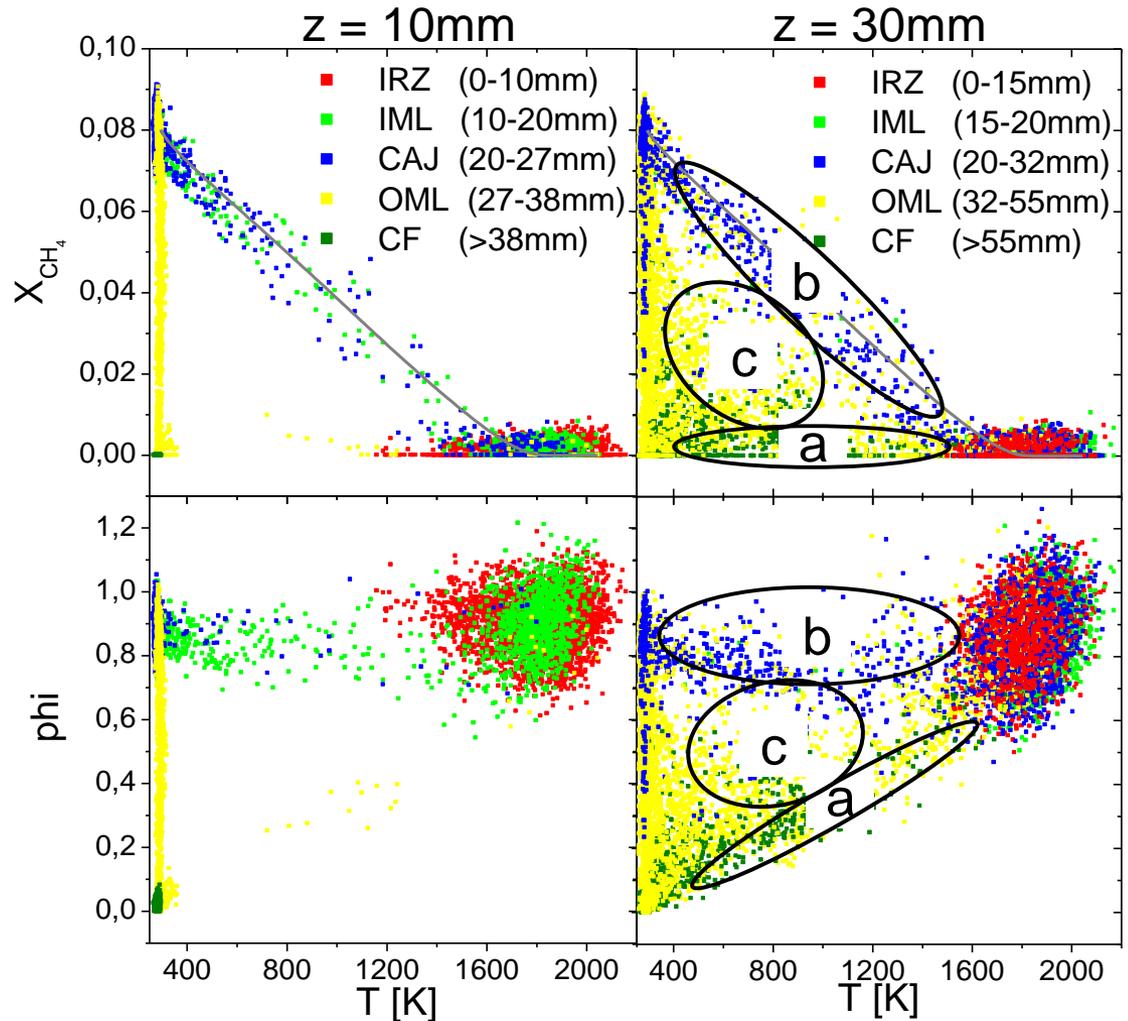
Single Shot Correlations - Scatter Plots

- **samples can be assigned to flame regions:**
 - **inner recirculation zone** (0-10mm):
fully burnt samples @ max T, no secondary air
 - **inner mixing layer & central annular jet** (10-27mm):
burnt, unburnt or mixed samples, no secondary air
 - **outer mixing layer** (27 - 38 mm):
mostly unburnt fuel and / or secondary air
rarely mixing between burnt samples and secondary air
 - **coflow / flange** (>38 mm):
exclusively ambient air



Scatter Plots - z Dependency

- at $z = 30$ mm:
- significantly increased probability to measure intermediate samples due to:
 - a) secondary air entrainment into burnt exhaust (OML, CF)
 - b) mixing between burnt / unburnt fuel (CAJ) and reaction without dilution
 - c) mixing of air with reacted AND unreacted fuel
- or
- slowed or extinguished reactions (CAJ, OML, CF)



Conclusions Raman/Rayleigh scattering in swirling premixed flame



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- Temperature is key-quantity (reaction progress)
- Thermo-kinetic state precisely measured
- Thermo-kinetic state is a prerequisite for understanding pollutant formation and finite rate chemistry effects
- Main findings are
 - In region of flame stabilization ($z < 30$ mm) premixed flame front is not located in areas of stratification but in areas of almost constant ϕ
 - typical reaction and / or mixing behavior can be assigned to different flame regions
 - intermediate reaction states are promoted by dilution with air
 - distinction between pure mixing and local flame quenching needs additional diagnostics monitoring intermediate species