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Structure and Dynamics of Combustion Waves in Premixed Gases

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Lecture XIV Nonlinear dynamics of shock waves. Triple point and Mach stem formation.

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Lecture 14: Nonlinear dynamics of shock waves Mach stem formation

14-1. Experimental and DNS results

What is a Mach stem ? Mach stems and cellular detonations Spontaneous formation of Mach stems

14-2. Multidimensional dynamics of shock fronts

Linear dynamics Weakly nonlinear analysis

14-3. Shock-vortex interaction Formulation Analysis of the crossover

14-4. Shock-turbulence interaction Composite solution Model equation Comparison with DNS

XIV-I) Introduction. Recent experimental and DNS results

What is a Mach stem ?

Triple point = 3 shock waves + 1 slip line (degenerescence of shear layer) called also contact line discontinuity (Courant Friedrichs 1948)

First observed during the reflection of an oblique shock front incident an a wall



example of a triple point propagating in a uniform flow

Mach stems and cellular detonations

Experimental observations of the cellular structure of detonations

Transverse structures of gaseous detonations have been observed for a long time





Joubert et al (2008)



Shchelkin Troshin (1965)



markings left on soot-coated foils on the walls trajectory of triple points

visualisation of the cellular structures by optical methods



Nonlinear mechanisms



trajectory of Mach stems = makings



Mach stems propagating in the transverse direction



P.Clavin XIV **Spontaneous formation of Mach stems on shock fronts**

Schlieren experiments in shock tubes



5



Comparison with experiments 8 cm Denet et al 2015 0.08

0.06

0.10

0.12 0.14

Spontaneous formation of Mach stems

The incoming shock wave is not strong, $M_u = 1.5$ and the amplitude of wavy wall is small 1 mm Immediately after reflection the wrinkled reflected shock has a smooth sinusoidal form

Singularity of slope is formed spontaneously at about 15 μ s leading to triple points clearly observed as early as 20 μ s



Sufficiently far from the wall the wall effect becomes negligible

The shock is quasi-planar with Mach stems propagating in the transverse direction $\frac{1}{6}$ crossing each other without deformation as solitons are known to do $\frac{1}{6}$

P.Clavin XIV XIV-2) Multidimensional dynamics of shock fronts

Analysis for strong shocks in the Newtonian limit

Linear dynamics

Distinguished limit

In order to simplify the presentation the analysis is performed for strong shock in the Newtonian limit

$$\overline{M}_{u}^{2} \gg 1, \qquad (\gamma - 1) \ll 1,$$

$$\overline{M}_{u}^{2}(\gamma - 1) = O(1), \qquad \overline{M}_{N}^{2} \approx (\gamma - 1)/2 + 1/\overline{M}_{u}^{2} \ll 1,$$

$$\epsilon^{2} \equiv M_{N}^{2} \ll 1 \qquad \overline{M}_{u} = O(1/\epsilon), \qquad (\gamma - 1) = O(\epsilon^{2})$$

$$\overline{u}_{N}/\overline{\mathcal{D}} \approx \epsilon^{2}, \qquad \overline{a}_{N}^{2} \approx \overline{u}_{N}\overline{\mathcal{D}}, \qquad \overline{a}_{N}/a_{u} = O(1)$$

in the frame of the unperturbed planar shock

$$M = \mathcal{D}/a$$
initial fluid shocked fluid, Neumann state
$$\begin{array}{c|c} \mathcal{D} > a_u \\ \hline \mathcal{D} > a_u \\ \hline \mathcal{M}_u > 1 \\ (p_u, \rho_u) \\ x = 0 \end{array} \xrightarrow{K} \begin{array}{c} \mathcal{M}_N < 1 \\ (\overline{p}_N, \overline{\rho}_N) \\ x = 0 \end{array}$$

Rankine-Hugoniot relations (see p. 6 & p.9 lecture XIII)

$$\frac{\delta p_N}{\overline{p}_N} \approx -2\frac{\dot{\alpha}_t}{\overline{\mathcal{D}}}, \qquad \frac{\delta \rho_N}{\overline{\rho}_N} = -2\left(\frac{\overline{a}_u}{\overline{a}_N}\right)^2 \frac{\dot{\alpha}_t}{\overline{\mathcal{D}}},$$
$$(\delta u_N - \dot{\alpha}_t) = -\frac{\left[(\gamma - 1)\overline{M}_u^2 - 2\right]}{2\overline{M}_u^2}\dot{\alpha}_t, \qquad \delta w_N \approx \overline{\mathcal{D}}\alpha'_y,$$

where for simplicity some unimportant ϵ^2 terms have been omitted in δp_N and δw_N

Quasi-isobaric approximation of the flow in the shocked gas





the acoustic waves propagates in a direction quasi-parallel to the front

P.Clavin XIV



the acoustic waves are negligibly smaller than the vorticity wave

$$|\delta u^{(i)}/\delta w^{(i)}| = O(\epsilon)$$

 $\overline{a}_N \delta t$

 $\overline{u}_N \delta t$

the vorticity wave is a shear flow quasi-parallel to the front propagating at a subsonic velocity in the normal direction

$$\begin{pmatrix} \frac{\partial}{\partial t} + \overline{u}_N \frac{\partial}{\partial x} \end{pmatrix} \mathbf{u}^{(i)} = 0 \implies \delta u^{(i)} = \dot{\alpha}_t (y, t - x/\overline{u}_N) \qquad \delta w^{(i)} = \overline{\mathcal{D}} \alpha'_y (y, t - x/\overline{u}_N)$$

$$\frac{\partial u^{(i)}}{\partial x} + \frac{\partial w^{(i)}}{\partial y} = 0 \implies -\frac{1}{\overline{u}_N} \frac{\partial^2 \alpha}{\partial t^2} + \overline{\mathcal{D}} \frac{\partial^2 \alpha}{\partial y^2} = 0 \qquad \overline{u}_N \overline{\mathcal{D}} \approx \overline{a}_N^2 \implies \text{Wave equation}$$

A subsonic wave that is sufficiently tilted yields a trace on the front that is sonic

Weakly nonlinear analysis

Clavin (2013)

Nonlinear Euler equations

$$\frac{\partial u}{\partial t} + \overline{u}_N \frac{\partial u}{\partial x} = \mathcal{U} - \frac{1}{\rho} \frac{\partial p}{\partial x}, \qquad \frac{\partial w}{\partial t} + \overline{u}_N \frac{\partial w}{\partial x} = \mathcal{W} - \frac{1}{\rho} \frac{\partial p}{\partial y}, \\
\frac{u^{(i)} = \overline{\nu} \alpha'_y(y, t - x/\overline{u}_N)}{\overline{\nu} \overline{u}_N \approx \overline{a}_N^2} \\
\frac{\overline{\nu} u}{\overline{u}_t = \overline{a}_N^2 \alpha''_{y^2}} \qquad \qquad -\mathcal{U} \equiv \delta u \frac{\partial u}{\partial x} + w \frac{\partial u}{\partial y}, \qquad -\mathcal{W} \equiv \delta u \frac{\partial w}{\partial x} + w \frac{\partial w}{\partial y}, \qquad \text{where} \qquad \frac{\delta u \equiv u - \overline{u}_N \approx u^{(i)}}{w \approx w^{(i)}} \\
\mathcal{U} = O(\varepsilon \partial u^{(i)} / \partial t) \qquad \qquad \mathcal{W} = O(\varepsilon \partial w^{(i)} / \partial t) \\
\text{where} \quad \varepsilon \equiv |\dot{\alpha}_t| / \overline{u}_N = O(|\alpha'_y| \overline{a}_N / \overline{u}_N) \quad \text{that is} \quad \boxed{\varepsilon = O(|\alpha'_y|/\epsilon)}$$

The weakly nonlinear approximation is valid when the nonlinear terms \mathcal{U} and \mathcal{V} are small (compared with the linear terms) This is the case for small amplitudes of the wrinkles $|\alpha'_y| \ll \epsilon$ where $\epsilon \equiv \overline{M}_N = \overline{u}_N / \overline{a}_N$ namely for $\varepsilon \ll 1$

Perturbation analysis for $\varepsilon \ll 1$

where
$$\mathcal{U} \approx \frac{1}{2} \frac{\partial H}{\partial x}, \quad \mathcal{W} \approx -\frac{1}{2} \frac{\overline{\mathcal{D}}}{\overline{u}_N} \frac{\partial H}{\partial y},$$

 $H \equiv [-\dot{\alpha}_t^2(y, t - x/\overline{u}_N) + \overline{a}_N^2 \alpha_y^{'2}(y, t - x/\overline{u}_N)].$

progressive wave: $\dot{\alpha}_t = \pm \overline{a}_N \alpha'_y \quad \Rightarrow \quad H = 0, \quad \mathcal{U} = 0, \quad \mathcal{V} = 0$

the shear wave $u^{(i)} = \dot{\alpha}_t(y, t - x/\overline{u}_N) \quad w^{(i)} = \overline{\mathcal{D}}\alpha'_y(y, t - x/\overline{u}_N)$ is an exact solution of the Euler equations for p = 0

the first order correction terms should come from the boundary conditions at $x = \alpha(y, t)$ (Rankine-Hugoniot)

Limiting the attention to the nonlinear corrections of order $\varepsilon \equiv |\alpha'_y|/\epsilon$ the Rankine-Hugoniot conditions yield



The shift of the front position also introduces quadratic terms

$$x = 0$$
: $\delta u \equiv u_f(y, t) \approx \delta u_N - \alpha u'_x$, $w \equiv w_f(y, t) \approx w_N - \alpha w'_x$

The nonlinear equations for the wrinkles is obtained from the incompressible condition

$$-\overline{u}_N^{-1}\partial u_f/\partial t + \partial w_f/\partial y = 0$$

 $H = 0 \implies$ the nonlinear terms coming from shift of the front position do not contribute

$$-\overline{u}_{N}\partial(\alpha u_{x}')/\partial t + \partial(\alpha w_{x}')/\partial y = 0$$

$$-\frac{1}{\overline{u}_{N}}\frac{\partial u_{N}}{\partial t} + \frac{\partial w_{N}}{\partial y} = 0 \quad \Rightarrow \boxed{\frac{\partial^{2}\alpha}{\partial t^{2}} - \overline{a}_{N}^{2}\frac{\partial^{2}\alpha}{\partial y^{2}} + \overline{\mathcal{D}}\frac{\partial}{\partial t}\left(\frac{\partial\alpha}{\partial y}\right)^{2} = 0}_{\sqrt{1}} \qquad (\overline{a}_{N}^{2} \approx \overline{\mathcal{D}}\overline{u}_{N})$$
nonlinear correction of order ε , $\overline{\mathcal{D}}\alpha_{y}'^{2}/|\dot{\alpha}_{t}| \approx (\overline{\mathcal{D}}/\overline{a}_{N})|\alpha_{y}'| \approx \varepsilon$

nonlinear correction of order ε , $\overline{\mathcal{D}}\alpha_{y}^{'2}/|\dot{\alpha}_{t}| \approx (\overline{\mathcal{D}}/\overline{a}_{N})|\alpha_{y}'| \approx \varepsilon$ Mach stem formation

$$\frac{\partial^2 \alpha}{\partial t^2} - \overline{a}_N^2 \frac{\partial^2 \alpha}{\partial y^2} + \overline{\mathcal{D}} \frac{\partial}{\partial t} \left(\frac{\partial \alpha}{\partial y} \right)^2 = 0$$

Two timescales problem: wavelength of the wrinkles
short time
$$\tau_s \equiv L/\overline{a}_N$$
 (period of oscillation)
long time $\tau_l \equiv \tau_s/\varepsilon$ (for the formation of a singularity of slope)
Non-dimensional form $t \equiv t/\tau_s$, $y \equiv y/L$, $A \equiv \alpha/(\varepsilon \epsilon L)$
 $\frac{\partial^2 A}{\partial t^2} - \frac{\partial^2 A}{\partial y^2} + \varepsilon \frac{\partial}{\partial t} \left(\frac{\partial A}{\partial y}\right)^2 = 0$
small nonlinear correction term producing a singularity at finite (but long) non-dimensional time $1/\varepsilon$, $t = O(1/\varepsilon$
that is at the long timescale $t = O(\tau_l)$
so that A may be considered to depend on two reduced time variables t and $t' \equiv \varepsilon t$, $\begin{cases} \frac{\partial}{\partial t} \rightarrow \frac{\partial}{\partial t} + \varepsilon \frac{\partial}{\partial t} \\ \frac{\partial^2}{\partial t^2} - \frac{\partial^2}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial^2}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial^2}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial^2}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial^2}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t} \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} - \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2} + z \frac{\partial}{\partial t^2} \\ \frac{\partial}{\partial t^2}$

different only by a numerical factor 1/2



XIV-3) Shock-vortex interaction Formulation

Clavin (2013)

 \overline{a}_N

 $\overline{a}_N t$

strong shock + weak vortex

 $\epsilon^2 \equiv M_N^2 \ll 1 \qquad \overline{M}_u = O(1/\epsilon), \qquad (\gamma - 1) = O(\epsilon^2)$

Consider a cylindrical and very subsonic vortex of diameter L and turnover velocity v_e , $v_e/\overline{a}_u \ll \epsilon$ $(v_e \ll \overline{a}_u/\overline{M}_u)$ Interaction time $\tau_{int} = L/\overline{\mathcal{D}} \ll$ turnover time $L/v_e \Rightarrow$ frozen flow $u_e(\mathbf{r}) w_e(\mathbf{r}) +$ small disturbances of the front The disturbances of the front during the crossover can be described by a linear analysis Interaction time $\tau_{int} = L/\overline{\mathcal{D}} \ll$ propagation time in the transverse direction of the wrinkles L/\overline{a}_N After the interaction time, $t > \tau_{int}$, the wrinkled shock front propagates in a quiescent medium 2 timescales: short crossover and longer transverse propagation of the wrinkles

the crossover provides the initial conditions

Linear analysis of the crossover

 $\overline{\mathcal{D}}$ $\overline{a}_N + \overline{u}_N$ Similar analysis but with an upstream flow Transmitted vortex Strong $\delta u_1(\mathbf{r},t), \quad \delta w_1(\mathbf{r},t), \quad \delta p_1(\mathbf{r},t)$ Initial acoustic vortex burst Rankine-Hugoniot (generalization of the relations p. 6) $\overline{a}_N t$ $\overline{u}_N t$ (the subscript f denotes the value at the shock front of the upstream flow) squeezed vortex $\frac{\delta p_N}{\overline{p}_N} - \frac{\delta p_{1f}}{\overline{p}_u} \approx 2 \frac{(\delta u_{1f} - \dot{\alpha}_t)}{\overline{\mathcal{D}}}, \quad \frac{\delta \rho_N}{\overline{\rho}_N} - \frac{\delta \rho_{1f}}{\overline{\rho}_u} = 2 \left(\frac{\overline{a}_u}{\overline{a}_N}\right)^2 \frac{(\delta u_{1f} - \dot{\alpha}_t)}{\overline{\mathcal{D}}},$ by compression $\overline{u}_N \ll \overline{\mathcal{D}}$ $\left(\delta u_N - \dot{\alpha}_t\right) = \frac{\left[(\gamma - 1)\overline{M}_u^2 - 2\right]}{2\overline{M}^2} \left(\frac{\delta u_{1f}}{\delta u_{1f}} - \dot{\alpha}_t\right), \quad \delta w_N \approx \overline{\mathcal{D}}\alpha'_y + \frac{\delta w_{1f}}{\delta w_{1f}},$ $\delta u_{1f}(y,t) = u_e|_{x=-\overline{\mathcal{D}}t}, \quad \delta w_{1f}(y,t) = w_e|_{x=-\overline{\mathcal{D}}t}, \quad \delta p_{1f}(y,t) = p_e|_{x=-\overline{\mathcal{D}}t}$

Acoustic burst

Acoustic in the shocked gases (Doppler neglected for simplicity) $0 < t < \tau_{int}$

$$\begin{aligned} \frac{\partial u^{(a)}}{\partial t} \approx -\frac{1}{p_{N}} \frac{\partial p}{\partial x}, \quad \frac{\partial w^{(a)}}{\partial t} \approx -\frac{1}{p_{N}} \frac{\partial p}{\partial y}, \quad \frac{\partial^{2} p}{\partial t^{2}} \approx \overline{a}_{N}^{2} \left(\frac{\partial^{2} p}{\partial x^{2}} + \frac{\partial^{2} p}{\partial y^{2}} \right) \\ x = 0, \quad 0 < t < \tau_{int}: \quad \partial/\partial t = O(\overline{D}/L), \quad \partial/\partial y = O(1/L) \end{aligned}$$
A quasi-planar and longitudined pressure burst of transverse extension L is generated $\overline{a_{N}} = \frac{\partial p}{\partial x} \approx (1/\overline{a}_{N}) \partial p/\partial t \approx (\overline{D}/\overline{a}_{N}) \delta p/L \approx \epsilon^{-1} (\partial p/\partial y) \Rightarrow |\delta w^{(a)}|/|\delta u^{(a)}| = O(\epsilon) \xrightarrow{\pi_{N}} \frac{\pi_{N}}{p_{N}} = \frac{\pi_{N}}{p_{N}} \frac{\partial p}{p_{N}} \approx \frac{2(k/\overline{a}_{N})^{2}}{p_{N}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})}{c} \ll \frac{(v_{e}/\overline{a}_{N})}{c} \ll \frac{1}{2(\overline{a}_{N}/\overline{D})(\delta u_{1f})} - \dot{\alpha}_{t}) \xrightarrow{\pi_{N}} \frac{(v_{e}/\overline{a}_{N})}{a_{N}t} = \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \times \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{(\overline{a}_{N}/\overline{D})(\delta u_{1f})} = \dot{\alpha}_{t} \xrightarrow{\pi_{N}} \frac{(v_{e}/\overline{a}_{N})}{a_{N}t} \times \frac{(v_{e}/\overline{a}_{N})^{2}}{a_{N}t} \times \frac{(v_{e}/\overline{a}_{N})^{2}}{\omega_{N}t} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{v_{e}/\overline{D}} \approx \frac{(v_{e}/\overline{a}_{N})^{2}}{(\overline{a}_{N}/\overline{D})(\delta u_{1f})} = \dot{\alpha}_{t} \xrightarrow{\pi_{N}} \frac{(v_{e}/\overline{a}_{N})^{2}}{a_{N}t} \times \frac{(v_{e}/\overline{a}_{N})^{2}}{\omega_{N}t} \times \frac{(v_{e}/\overline{a}_{N})^{2}}{\omega_{N}t} \times \frac{(v_{e}/\overline{a}_{N})^{2}}{(\overline{a}_{N}/\overline{D})(\delta u_{1f})} = O(\frac{\overline{a}}{\overline{a}_{N}}) \xrightarrow{\pi_{N}} \frac{(v_{e}/\overline{a}_{N})^{2}}{\omega_{N}t} \times \frac{(v_{e}/$

of the vortex velocity

Wrinkles of very small amplitude are left on the shock front by the vortex

$$|\alpha| = O(\epsilon^2 L v_e / \overline{a}_u), \qquad |\alpha'_y| = O(\epsilon^2 v_e / \overline{a}_u)$$

XIV-4) Shock-turbulence interaction

Strong shock propagating in a weakly turbulent flow

Composite solution for a single vortex

During crossover

$$v_e/\overline{a}_u \ll \epsilon, \ 0 < t < \tau_{int}: \quad \dot{\alpha}_t \approx 2(\overline{a}_N/\overline{\mathcal{D}})\delta u_{1f}, \quad \alpha(y,t) = 2\frac{\overline{a}_N}{\overline{\mathcal{D}}} \int_{-\overline{\mathcal{D}}t}^0 \mathrm{d}x \frac{u_e(x,y)}{\overline{\mathcal{D}}}$$

beginning of interaction < t < end of interaction :

$$\frac{\partial^2 \alpha}{\partial t^2} \approx 2 \frac{\overline{a}_N}{\overline{\mathcal{D}}} \frac{\partial \delta u_{1f}}{\partial t}$$

valid during a short lapse of time of order $L/\overline{\mathcal{D}}$

$$\frac{\partial^2 \alpha}{\partial t^2} - \overline{a}_N^2 \frac{\partial^2 \alpha}{\partial y^2} + \overline{\mathcal{D}} \frac{\partial}{\partial t} \left(\frac{\partial \alpha}{\partial y} \right)^2 \approx 0$$

involves a time scale of evolution L/\overline{a}_N longer than $L/\overline{\mathcal{D}}$ $\epsilon = \overline{a}_N/\overline{\mathcal{D}} \ll 1$

Composite equation

$$\frac{\partial^2 \alpha}{\partial t^2} - \overline{a}_N^2 \frac{\partial^2 \alpha}{\partial y^2} + \overline{\mathcal{D}} \frac{\partial}{\partial t} \left(\frac{\partial \alpha}{\partial y}\right)^2 = 2 \frac{\overline{a}_N}{\overline{\mathcal{D}}} \frac{\partial \delta u_{1f}}{\partial t} \checkmark$$

frozen velocity field $u_e(x, y)$ $\delta u_{1f}(y, t) = u_e|_{x=-\overline{D}t}$ short living forcing term

taking advantage of the two different time scales

Model equation

Extension to 3 dimensions

$$\times \left(\frac{L\overline{\mathcal{D}}}{\overline{a}_{N}^{3}}\right) \qquad \qquad \frac{\partial^{2}\alpha}{\partial t^{2}} - \overline{a}_{N}^{2}\Delta\alpha + \overline{\mathcal{D}}\frac{\partial|\nabla\alpha|^{2}}{\partial t} = 2\frac{\overline{a}_{N}}{\overline{\mathcal{D}}}\frac{\partial\delta u_{1f}}{\partial t}$$
where $\delta u_{N}(u, \alpha, t) = u_{N}(x, u, \alpha, t)$

where $\delta u_{1f}(y, z, t) = u_e(x, y, z, t)|_{x=-\overline{\mathcal{D}}t}$

 \searrow forcing term varying on the on the length scale L and on time scale $L/\overline{\mathcal{D}}$

non-dimensional form

$$\eta \equiv y/L, \qquad \zeta \equiv z/L, \qquad \tau \equiv \overline{a}_N t/L, \qquad \phi \equiv \alpha/(\epsilon L) \qquad \epsilon \equiv \overline{a}_N/\overline{\mathcal{D}}$$
$$\frac{\partial^2 \phi}{\partial \tau^2} - \Delta \phi + \frac{\partial |\nabla \phi|^2}{\partial \tau} = \frac{\partial \psi(\eta, \zeta, \tau/\epsilon)}{\partial \tau} \qquad \text{where} \quad \psi \equiv 2\left(\frac{\delta u_{1f}}{\overline{a}_N}\right) \qquad |\psi| = O(v_e/\overline{a}_N)$$

 ψ is a small term varying on the short (reduced) time scale ϵ and on the (reduced) length scale unity $\partial \psi / \partial \tau$ is a small (reduced) forcing term fluctuating rapidly $|\partial \psi / \partial \tau| = O(v_e / (\epsilon \overline{a}_u))$ $(v_e / \overline{a}_u \ll \epsilon)$

$Numerical\ results$

Denet (2015)

The characteristic cell size of the patterns at the shock front is much larger than the integral scale of the turbulence

The size of the patterns looks to grow with time Saturation by the box size ?

length scale of the turbulence at the shock front







Spectral analysis of the pattern size

Evolution of the spectra of the wrinkles of the front shock

The size of the pattern increases with time



Comparison with DNS



DNS Larson et al. (2013)



Model equation Denet (2015)

DNS shock-vortex interaction Vervisch Lodato (2015)









$$\overline{\mathcal{D}}/a_u = 2, \qquad v_e/a_u = 0.8, \qquad \gamma = 1.4$$

Two Mach stems are observed as in the model equation