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Structure and Dynamics of Combustion Waves in Premixed Gases

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Lecture X Supersonic waves

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Lecture 10 : Supersonic waves

10-1. Background

Model of hyperbolic equations for the formation of discontinuity Riemann invariants

Rankine-Hugoniot conditions for shock waves

Mikhelson (Chapman-Jouguet) conditions for detonations

10-2. Inner structure of a weak shock wave

Formulation Dimensional analysis Analysis

10-3. ZND structure of detonations

10-4. Selection mechanism of the CJ wave

X-I) Background

shock wave \approx discontinuity in the solution of the Euler equations



Model of hyperbolic equations for the formation of discontinuities

$$a(u) \qquad \qquad \frac{\partial u/\partial t + a(u)\partial u/\partial x = 0}{u = u(x, t) ?}$$

Simple case: linear equation

$$a = a_o = \operatorname{cst.}$$

$$u = u_o(x - a_o t)$$

propagation at constant velocity without deformation

Nonlinear equation $a(u) \quad da/du \neq 0$

Method of characteristics

The solution is conserved along any trajectory dx/dt = a(u) in the phase plan (x, t). u = u(x(t), t) $\frac{du}{dt} = 0$ $u(x, t) = \text{cst.} \Rightarrow a(x, t) = \text{cst.}$

u(x,t) is constant along the straight lines $x = a_o t + x_o$: $u = u_o$

 $\partial u/\partial t + a(u)\partial u/\partial x = 0$

$$t = 0: \quad u = u_o(x) \qquad \qquad u = u(x, t) ?$$



Method of characteristics

The solution is conserved along any trajectory dx/dt = a(u) in the phase plan (x, t). u(x,t) is constant along the straight lines $x = a_o t + x_o : u = u_o$ $u_o \uparrow$ Speed increases with increasing u, $\frac{\mathrm{d}a}{\mathrm{d}u} > 0$ formation of singularities after a finite time larger values run faster " $t > t_b$ $t = t_b$ $t > t_b$: characteristics intersect $t > t_b$: multivalued solution. Wave breaking $u(x,t) = u_o(x_o(x,t)), \quad x(x_o,t) = a_o(x_o)t + x_o, \quad \partial x/\partial x_o = 1 + t(\mathrm{d}a_o/\mathrm{d}x_o) \quad \partial x_o/\partial x = [1 + t(\mathrm{d}a_o/\mathrm{d}x_o)]^{-1}$ trajectory $\frac{\partial u}{\partial x} = \frac{\partial x_o}{\partial x} \frac{\mathrm{d} u_o}{\mathrm{d} x_o} \quad \frac{\partial u}{\partial x} = \frac{\overline{\mathrm{d} u_o/\mathrm{d} x_o}}{[1 + t(\mathrm{d} a_o/\mathrm{d} x_o)]} \quad \text{diverges at time} \quad t = \frac{1}{-\mathrm{d} a_o/\mathrm{d} x_o} \quad \text{where} \quad da_o/\mathrm{d} x_o < 0$ $t_b \equiv$ time of wave breaking (shortest time for the divergence of $\partial u / \partial x$) $t_b = \frac{1}{\max |\mathrm{d}a_0/\mathrm{d}x_0|}$

Discontinuous solutions

$$\begin{array}{cccc} \partial u/\partial t + a(u)\partial u/\partial x = 0 & \text{conservative form} & \partial u/\partial t + \partial j/\partial x = 0 & j(u) & dj/du = a(u) \\ \text{Are step functions } u_+ \neq u_-\text{propagating at constant velocity } \mathcal{D} \text{ solutions }? & u_- & u_-$$

a(u) = u: Burgers equation. Analytical solution to the initial value problem

Riemann invariants (1860)



P.Clavin X



shock wave at constant velocity > piston velocity

Centred waves

t < 0: piston velocity = 0

t > 0: piston velocity = cst $\neq 0$

Sel-similar solutions x/t



no discontinuity of u discontinuity of du/dx propagating at the local sound speed fully unsteady process: thickness $\int u_p t$

 ρ_u



Rankine-Hugoniot conditions for shock waves (1870 - 1880)

Rankine 1870 Hugoniot 1880

Eqs for the conservation of mass, momentum and energy

 $2 \setminus \rho_u$

 ρ

$$Ideal \ (polytropic) \ gas \ \gamma \equiv c_p/c_v$$

$$p = (c_p - c_v)\rho T, \qquad h = c_p T = \frac{\gamma}{\gamma - 1} \frac{p}{\rho}$$

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$$p = -m^2 \left(\frac{1}{\rho} - \frac{1}{\rho_u}\right)$$

$$\mathcal{P} \equiv \frac{(\gamma + 1)}{2\gamma} \left(\frac{p}{p_u} - 1\right), \quad \mathcal{V} \equiv \frac{(\gamma + 1)}{2} \left(\frac{\rho_u}{\rho} - 1\right)$$

$$(\mathcal{P} + 1)(\mathcal{V} + 1) = 1 \qquad \mathcal{P} = -M_u^2 \mathcal{V}$$

$$Hugoniot \ curve \qquad Michelson-Rayleigh \ line$$

$$quadratic \ equation \ for \ \mathcal{V}, \ 2 \ solutions: \ \mathcal{V} = 0, \ \mathcal{V} = \mathcal{V}_N$$

$$Shocked \ gas \ (Neumann \ state) \ vs \ M_u$$

$$\frac{u_N}{\mathcal{D}} = \frac{\rho_u}{\rho_N} = \frac{(\gamma - 1)M_u^2 + 2}{(\gamma + 1)M_u^2} \qquad \frac{p_N}{p_u} = \frac{2\gamma M_u^2 - (\gamma - 1)}{(\gamma + 1)} \qquad \frac{T_N}{T_u} = \frac{[2\gamma M_u^2 - (\gamma - 1)][(\gamma - 1)M_u^2 + 2]}{(\gamma + 1)^2 M_u^2} \qquad \text{Initial state} \qquad \rho_u \ \rho_$$

General comments

The Hugoniot curve is tangent to the isentropic

the entropy change along the Hugoniot curve is of third order $\implies M_u \equiv D/a_u > 1$

$$\delta s = s - s_u \qquad \delta p = p - p_u \\ \delta s \not \wedge \delta p \not \land \qquad \delta s = \frac{1}{12} \frac{1}{T_u} \left(\frac{\partial^2 (1/\rho)}{\partial p^2} \right)_s (\delta p)^3$$

The Hugoniot relation is not an iso-function of state

$$h(p,\rho) - h(p_u,\rho_u) - \frac{1}{2}\left(\frac{1}{\rho_u} + \frac{1}{\rho}\right)(p - p_u) = 0 \quad \text{cannot be written in the form} \quad \mathcal{H}(1/\rho,p) = \mathcal{H}(1/\rho_u,p_u)$$

$$h(p,\rho) - h(p_N,\rho_N) - \frac{1}{2}\left(\frac{1}{\rho_N} + \frac{1}{\rho}\right)(p - p_N) = 0 \quad \neq \quad h(p,\rho) - h(p_u,\rho_u) - \frac{1}{2}\left(\frac{1}{\rho_u} + \frac{1}{\rho}\right)(p - p_u) = 0$$

Rarefaction shock does not exist. The entropy of the fluid increases through the shock (Irreversibility) can be proved for weak shock by the entropy balance or by the H-theorem using the Boltzmann equation $\rho u \frac{ds}{dx} = \frac{d}{dx} \left(\frac{\lambda}{T} \frac{dT}{dx} \right) + \dot{\omega}_s \qquad \dot{\omega}_s > 0$



Mikhelson condition for the CJ detonation (1893)



 $(M_u^2 - 1)^2 \ge 4\mathcal{Q}M_u^2$ $M_u \ge M_{u_{CJ}} \equiv \sqrt{\mathcal{Q}} + \sqrt{\mathcal{Q} + 1},$ Mikhelson (1893)

In the CJ wave the velocity of the burned gas is sonic in the frame of the wave $u_{bCJ} = a_{bCJ}$ (self-sustained wave) (Rayleigh line is tangent)

In the overdriven detonations $\mathcal{D} > \mathcal{D}_{CJ}$ the velocity of the burned gas is subsonic in the frame of the wave $u_b < a_b$ (piston-supported detonation)





Paul Vieille (1900)

X-2) Inner structure of a weak shock

$$\frac{\partial p}{\partial t} + \frac{\partial (pu)}{\partial x} = 0 \qquad \frac{\partial (pu)}{\partial t} - \frac{\partial}{\partial x} \left(p + \rho a^2 - \mu \frac{\partial u}{\partial x} \right) \qquad \frac{\partial (\rho v_{tab})}{\partial t} = -\frac{\partial}{\partial x} \left[\rho u(h + u^2/2) - \lambda \frac{\partial T}{\partial x} - \mu u \frac{\partial u}{\partial x} \right] \qquad (p_N, \rho_N)$$
Formulation
(reference frame attached to the shock wave)
$$\rho u = m, \qquad p + \rho u^2 - \mu \frac{du}{dx} = \operatorname{cst.} \qquad m \left(h + \frac{u^2}{2} \right) - \lambda \frac{dT}{dx} - \mu u \frac{du}{dx} = \operatorname{cst.} \qquad \operatorname{shock thickness}$$

$$x \to -\infty: \quad p = p_u, \quad \rho = \rho_u, \quad u = \mathcal{D} \qquad x \to \infty: \quad dp/dx = 0, \quad dp/dx = 0, \quad du/dx = 0$$

$$\frac{p}{\rho} = (\gamma - 1)c_vT \qquad h = \frac{\gamma}{\gamma - 1} \frac{p}{\rho}$$
Two coupled equations for p and $v \equiv 1/\rho, m$ given $(u = mv, \quad c_vT = pv/(\gamma - 1))$

$$(p - p_u) + m^2(v - v_u) = \mu m \frac{dv}{dx},$$

$$\frac{\gamma}{\gamma - 1} (pv - p_u v_u) - \frac{1}{2} (p - p_u)(v + v_u) = \frac{\gamma}{\gamma - 1} \frac{\lambda}{mc_p} \frac{d(pv)}{dx} + \frac{\mu m}{2} (v - v_u) \frac{dv}{dx}$$

$$\frac{1}{2} (v + v_u) (v - v_u) - \frac{1}{2} (v + v_u) dv = 0$$
Dimensional analysis
$$u/d = O(1), \qquad \text{mean free path}$$

$$\mu/\rho = \text{viscous diffusion coefficient} \approx \ell/a \qquad \Rightarrow \text{ thickness of shock waves } \approx \text{ mean free path}$$

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$$\mu u = \frac{\rho u^2 \times \mu \frac{du}{dx}$$

$$M_u \equiv \mathcal{D}/a_u > 1$$
 Analysis for $\epsilon \equiv M_u - 1 \ll 1$ (weak shock)

$$v \equiv 1/\rho$$
 $\nu \equiv (v - v_u)/v_u = O(\epsilon)$ $\pi \equiv (p - p_u)/p_u = O(\epsilon)$

$$\begin{split} & \underset{\substack{(p-p_u)+m^2(v-v_u)=\mu m \frac{dv}{d\xi}, \\ \gamma = 1}}{\sum x/\ell} \underbrace{\int_{\substack{(p-p_u)+m^2(v-v_u)=\mu m \frac{dv}{d\xi}, \\ \gamma = 1}} O(\epsilon^3)}_{\substack{(p-p_u)-\frac{1}{2}(p-p_u)(v+v_u)=\frac{\gamma}{\gamma-1}\frac{\lambda}{m_p}\frac{d(p)}{d(x)}+\frac{\mu m}{2} \\ \text{anticipating}} \underbrace{\int_{\substack{(p-p_u)-\frac{1}{2}(p-p_u)(v+v_u)=\frac{\gamma}{\gamma-1}\frac{\lambda}{m_p}\frac{d(p)}{dx}+\frac{\mu m}{2} \\ \text{anticipating}} \underbrace{\int_{\substack{(p-p_u)-\frac{1}{2}(v-p_u)(v+v_u)=\frac{\gamma}{\gamma-1}\frac{\lambda}{m_p}\frac{d(p)}{d(x)}+\frac{\mu m}{2} \\ \frac{d\nu}{d\xi} = O(\epsilon^2) \\ d\pi/d\xi = O(\epsilon^2) \\ \begin{pmatrix} \frac{\gamma+1}{2\gamma} \\ \frac{\gamma}{2\gamma} \\ \frac{\gamma}{2\gamma$$

the Rankine-Hugoniot jumps at order ϵ are recovered when dissipative terms are neglected $\nu_N = -4\epsilon \frac{1}{\gamma+1}$ $\pi_N = -4\epsilon \frac{\gamma}{\gamma+1}$

x

Y

$$\xi = -\infty: \text{ initial state, } \nu = 0, \qquad \xi = +\infty: \text{ shocked gas, } \nu = \nu_N = -4\epsilon/(\gamma + \gamma + \gamma))$$
$$Y \equiv \frac{(\gamma + 1)}{4\epsilon}\nu \in [0, -1] \qquad \zeta \equiv \frac{2}{[(\gamma + 1) + \Pr]}\epsilon\xi = \frac{2}{[(\gamma + 1) + \Pr]}\frac{x}{(\ell/\epsilon)} \qquad \zeta = 0$$

$$\frac{\zeta = 1}{\epsilon} \nu \in [0, -1] \qquad \zeta \equiv \frac{2}{\left[(\gamma + 1) + \Pr\right]} \epsilon \xi = \frac{2}{\left[(\gamma + 1) + \Pr\right]} \frac{x}{(\ell/\epsilon)} \qquad \zeta = 0$$

$$\frac{\frac{dY}{d\zeta} = Y(Y+1) < 0}{\zeta = -\infty : Y = 0, \qquad \zeta = +\infty : Y = -1}$$

 $\zeta = \int \frac{\mathrm{d}Y}{Y(Y+1)} \qquad Y(\zeta) = -\frac{\mathrm{e}^{\zeta}}{\mathrm{e}^{\zeta}+1}$ shock thickness = mean free path/ $(M_u - 1)$ microscopic length if $M_u - 1 = O(1)$ macroscopic length if $(M_u - 1) \ll 1$

X-3) ZND structure of detonations Zeldovich (1940) Neumann (1942) Döring (1944)

Orders of magnitude

 ℓ

Detonation Front

Zoom

End of heat

release zone

Piston

velocity

N٠

Shock -

Detonation

velocity

$$\frac{E}{k_B T_N} \gg 1 \quad \Rightarrow \quad \frac{1}{\tau_r(T_N)} \approx \frac{e^{-E/k_B T_N}}{\tau_{coll}} \ll \frac{1}{\tau_{coll}} \qquad \qquad \frac{u_N}{a_N} = O(1), \quad d_N \equiv u_N \tau_r(N) \gg a_N \tau_{coll} \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \gg a_N \tau_{coll} \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \gg a_N \tau_{coll} \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \gg a_N \tau_{coll} \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv u_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_{coll}} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad d_N \equiv U_N \tau_r(N) \approx \frac{1}{\tau_r(N)} = O(1), \quad$$

thickness of the reaction zone \gg thickness of the lead (inert) shock

structure of the detonation: inert shock followed by a much larger reaction zone conjectured by Vieille (1900)

$$\frac{D_T}{d_N^2} \approx \frac{a_N^2 \tau_{coll}}{d_N^2} \approx \frac{\tau_{coll}}{(\tau_r(T_N))^2} \approx \frac{e^{-E/k_B T_N}}{\tau_r(T_N)} \ll \frac{1}{\tau_r(T_N)}$$

diffusion rate \ll reaction rate \Rightarrow diffusion terms are negligible

Formulation

$$Reference frame of the lead shock (x = 0)$$

$$\frac{d(\rho u)}{dx} = 0$$

$$\frac{dp}{dx} + \rho u \frac{du}{dx} = 0$$

$$\frac{dw}{dx} = \rho \frac{dw}{dx} + \rho \frac{dw}{dx} = 0$$

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X-4) Selection mechanism of the CJ wave

Rarefaction wave in the burnt gas when the piston is suddenly stopped





Speed of discontinuities in lab. frame