#### **Chapter 5: Gas-Phase Thermometry**

#### **TU Darmstadt, Germany Dept. of Mechanical Engineering Institute for Reactive Flows and Diagnostics**









## **Combustion: coupled sub-processes**



#### **Combustion**:

Energy conversion of chemically bound to thermal energy



→ Each of these sub-processes is significantly influenced by local gas temperatures

# Need for accurate and precise temperature measurements to understand combustion



- Temperature (gas) is key quantity with impact on
  - Chemical kinetics (Arrhenius-type reaction rates)
  - Gas density (equation of state)
  - Viscosity
  - Progress variable in premixed combustion

#### → Turbulence-chemistry interaction

- Understanding combustion requires knowledge of local temperatures (gas)
  - Accurately: no systematic error (ideally)
  - Precisely: low statistical error (low noise, ..)
  - Locally: due to non-linear dependency of sub-processes on temperature



#### Laminar vs. turbulent combustion



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- Laminar and stationary combustion
  - No temporal variation
  - Large spatial variation (across heat release zone)
  - → Resolution requirements
    - Time: none
    - Space: high, depends on pressure, fuel etc., method must alow for resolving smallest scales (ideally)
- **Turbulent** (statistically stationary) combustion
  - Large temporal variation
  - Large spatial variation (heat release zone, convection, mixt. preparation)
  - → Resolution requirements
    - Time: resolve Bachelor time-scales (ideally)
    - Space: resolve Bachelor length-scales (ideally)



#### Intrusive vs. non-intrusive sensing (1)

- Intrusive sensors
  - Thermocouples
  - Resistance thermometer
  - Major disadvantages
    - Systematic errors (heat conduction, thermal radiation losses, impact on flow, promoting catalytic reactions, ...)
    - Not sustainable (melting point, oxidation of metal)
    - Size:  $\sim$ mm  $\rightarrow$  spatial resolution too low for resolving Bachelor scales
    - Temporal response: first order system with large time-constants

#### $\rightarrow$ Not well suited for many applications in combustion research









### Intrusive vs. non-intrusive sensing (2)



- Non-intrusive sensors: based on spectroscopic methods
  - Thermal radiation: generally not applicable in gaseous flames, suitable for measuring particle temperatures if emissivity is known
  - Chemiluminescence (OH\*, CH\*,...): not in chemical equilibrium





### Intrusive vs. non-intrusive sensing (2)



- Non-intrusive sensors: based on spectroscopic methods
  - Thermal radiation: generally not applicable in gaseous flames, suitable for measuring particle temperatures if emissivity is known
  - Chemiluminescence (OH\*, CH\*,...): not in chemical equilibrium
  - Spectroscopic methods
    - Probing Boltzmann distribution of quantum states
    - Exploit temperature-dependent absorption or emission bands
    - Measuring density





### Intrusive vs. non-intrusive sensing (2)



- Non-intrusive sensors: based on spectroscopic methods
  - Thermal radiation: generally not applicable in gaseous flames, suitable for measuring particle temperatures if emissivity is known
  - Chemiluminescence (OH\*, CH\*,...): not in chemical equilibrium
  - Spectroscopic methods
    - Probing Boltzmann distribution of quantum states
    - Exploit temperature-dependent absorption or emission bands
    - Measuring density
- $\rightarrow$  Well suited for many applications in combustion research
- $\rightarrow$  There is not the single best method, but best choice depends on purpose
- **Disadvantage**: effort is high, needs expert knowledge, needs optical access



## **Spectroscopic methods – classification**



#### • Based on

• Boltzmann distribution

 $\frac{N_i}{N} = \frac{g_i \exp(-E_i / kT)}{\sum_j g_j \exp(-E_j / kT)} = \text{unique function of } T$   $g_i: \text{ degeneracy factor } E_i: \text{ energy quantum state; both from quantum mechanics}$  $\sum_{i=1}^{N_i} \sum_{j=1}^{N_i} \sum_{j=1}^$ 

• Temperature-dependent absorption/emission

• Density (N/V) measurements  

$$pV = NkT \rightarrow T = \frac{pV}{Nk}$$
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#### **Restriction to diatomic molecules**

- Two atoms, covalent bounded
- Degrees of freedom
  - 3 translation
  - Electronic (here only valence electron considered)
  - 1 vibrational
  - 2 rotational (degenerated)
- In combustion degrees of freedom not necessarily in equilibrium!
- → Translational, electronic, vibrational, and rotational temperatures not always identical

Source: Wiley and Sons



Source: Wikipedia







#### Internal energies of diatomic molecule





Rotational sub-levels not shown

$$T = T^{el} + S(v, J) = T^{el} + G(v) + F(v, J)$$
  
=  $T^{el} + \omega_e \left(v + \frac{1}{2}\right) - \omega_e x_e \left(v + \frac{1}{2}\right)^2 + \omega_e y_e \left(v + \frac{1}{2}\right)^3 + \dots + B_v J(J+1) - D_v J^2 (J+1)^2 + \dots$ 

#### **Temperature measurement via Boltzmann (1)**

- Boltzmann distribution (diatomic molecule)
  - Rotational sub-levels

 $\frac{N_J}{N} = \frac{\left(2J+1\right)\exp\left(-E_J/kT\right)}{\sum_J \left(2J+1\right)\exp\left(-E_J/kT\right)}$ 

with J rotational quantum number

(fractional population)

 Already at T = 300 K many rotational sub-levels populated because energy separation between adjacent small (10 – 100 cm<sup>-1</sup>)





#### **Temperature measurement via Boltzmann (2)**



- Boltzmann distribution (diatomic molecule)
  - Vibrational sub-levels

$$\frac{N_{v}}{N} = \frac{\exp(-E_{v} / kT)}{\sum_{v} \exp(-E_{v} / kT)}$$

with v vibrational quantum number

Vibrationally excited levels n

Example  $N_2$ :

Energy gap between
 v"=0 and v'=1 ~2300 cm<sup>-1</sup>



#### **Temperature measurement via Boltzmann (3)**



- Boltzmann distribution (diatomic molecule)
  - Electronic sub-levels

 $\frac{N_{ES}}{N} = \frac{\exp(-E_{ES} / kT)}{\sum_{ES} \exp(-E_{ES} / kT)}$  with *ES* quantum number of electronic state

- Energy separation > 10000 cm<sup>-1</sup>
- → In general: Not significantly populated at combustion temperatures Exception: Atomic tracer such as indium (not considered in detail during this lecture)

 $\rightarrow$ Measure temperature via the distribution of rotational quantum states



### **Rotational temperatures – by microwaves**



- Task: measuring Boltzmann distribution of rotational sub-levels
  - Single photon resonant processes
  - Pure rotational spectroscopy



- Energy separation: 10 100 cm<sup>-1</sup> → microwave radiation
- $\rightarrow$  **Not common** in combustion (low spatial res., background radiation)



#### **Rotational temperatures – by IR spectroscopy**



Rotational-vibrational spectroscopy

- Energy separation: ~1000 4160 cm<sup>-1</sup> → infrared radiation
- Example HCI absorption spectrum





## Selection rules



- Fundamental finding from quantum mechanics
  - Change of vibrational quantum number  $\Delta v = \pm 1, \pm 2, ...$ •
  - Change of rotational quantum number  $\Delta J = \pm 1$ •
  - But exceptions (for example NO)  $\Delta J = 0, \pm 1$ •
  - Notation •

 $\Delta J = 0 \Longrightarrow$  Q-lines  $\Delta J = 1 \Rightarrow$  R-lines  $\Delta J = -1 \Rightarrow$  P-lines





# **Spectrum interpretation HCI**







# Rotational temperatures by UV/VIS spectroscopy (1)



- Electronic spectroscopy: change of electronic, vibrational and rotational states due to absorption of UV or VIS photon
  - Energy separation > 10000 cm<sup>-1</sup>
  - Selection rules (extract only)

 $\Delta J = 0, \pm 1 \rightarrow \text{Q-, R-, P- lines}$ 

 $\Delta v = 0, \pm 1, \pm 2, \dots \rightarrow$  Compare "Franck-Condon principle"

 $\rightarrow$  For Hund case (a) (most important rules)

- $\Delta \Lambda = 0, \pm 1 \qquad \Sigma \Sigma, \Pi \Sigma \text{ or } \Delta \Pi \text{ transitions. Not allowed for} \\ \text{example } \Delta \Sigma \text{ transitions}$
- $\Delta S = 0$  Allowed: Triplett Triplett or Singulett Singulett transitions Spin forbidden: Singulett – Triplett transitions

 $\Lambda$ :Projection of orbital momentum *L* on molecule axis

S: Multiplicity

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# Rotational temperatures by UV/VIS spectroscopy (2)



Electronic spectroscopy:



# Rotational temperatures by UV/VIS spectroscopy (3)



- OH  $A^2\Sigma \leftarrow X^2\Pi$  (v'=1  $\leftarrow$  v''=0)-transition
- R-branch, band head



# Methods in the IR & UV/VIS for temperature measurements via Boltzmann distribution



- Laser absorption spectroscopy (LAS)
- Laser-induced fluorescence (LIF)
- Raman spectroscopy (RS)
- Coherent anti-Stokes Raman spectroscopy (CARS)



## Laser absorption spectroscopy (1)



• Experimental setup



Deduce number densities from Beer-Lambert's law

$$I(x = L) = I_{0} \exp(-x \cdot N_{j} \cdot \sigma_{j \leftarrow i}) \Leftrightarrow N_{j} = \frac{\ln(\frac{I(x = L)}{I_{0}})}{x \cdot \sigma_{j \leftarrow i}}$$



# Laser absorption spectroscopy (2)



- Deduce temperature from Boltzmann distribution
  - Two-line thermometry

$$T = \frac{E_{J_2} - E_{J_1}}{k \ln\left(\frac{N_1(2J_2 + 1)}{N_2(2J_1 + 1)}\right)}$$

• Multi-line thermometry: by spectral fit





# Laser absorption spectroscopy (3)



- Advantages
  - Sensitive
  - Accurate (no calibration required if spectroscopic details such as term values, line strengths, line broadening mechanisms known)
  - High accuracy, needs multi-line thermometry (for instantaneous Tmeasurements these requires rapid tuning of laser frequency and fast detection)
  - High spatial resolution perpendicularly to laser path
- Disadvantages
  - Line-of-sight (LOS): no spatial resolution along laser path, needs homogeneous distribution along laser path
  - Multi-line thermometry needs fast tuning of laser and fast detector

#### $\rightarrow$ Great in laminar flames, not easily applicable in turbulent flames (LOS)



#### Laser Induced fluorescence (1)

Step 1: Absorption

- Electronic excitation of molecules by laser radiation
- Wavelength  $\lambda_A$

Step 2: Spontaneous emission (fluorescence)

- Spectrally red-shifted  $\lambda_A < \lambda_E$
- Upper state lifetime typically few ns for flame conditions
- Measure of local number density
- Linear LIF regime

$$I_{LIF}(\mathbf{x}) = N_{1}(\mathbf{x})\sigma\gamma(\mathbf{v})I_{laser}(\mathbf{x})\frac{\tau_{tot}}{\tau_{sp}}U\frac{\Omega}{4\pi}\varepsilon\eta$$











## Laser Induced fluorescence (3)



- Flame front visualization in CH<sub>4</sub>/air Bunsen flame, p = 1 bar
- Excitation by tunable KrF excimer laser at ~248 nm





# **Laser Induced fluorescence (4)**



- **Two-line** thermometry:
  - excite two different transitions
  - Transitions selected such that ratio of number densities  $N_1$  and  $N_2$  vary sensitively with temperature
  - But: number density should not be too low for reasonable signal-tonoise ratio
- Calculate ratio of two LIF Signals  $I_{LIF,j}(x \in N_i \times U(\alpha))_{laser,i} \times \gamma \vee \frac{\tau_{tot}}{\tau_{sp}} \frac{\Omega}{4\pi} \varepsilon \eta$  $\rightarrow$  Yield **ratio**

$$R_{12} = \frac{I_{L/F,1}}{I_{L/F,2}} = \frac{C_1 I_{laser,1} g_1 \exp(-E_1/kT) B_1 \gamma_1(\rho,T) \tau_{eff,1}/\tau_{sp,1}}{C_2 I_{laser,2} g_2 \exp(-E_2/kT) B_2 \gamma_2(\rho,T) \tau_{eff,2}/\tau_{sp,2}}$$

 $\rightarrow$  Issue two-line thermometry: Low precision due to experimental noise



# Laser Induced fluorescence (5)



- Multi-line thermometry: measure entire excitation-fluorescence spectrum
- Method 1: Spectral fit of entire spectrum by variation of temperature
- Method 2: Plot ln(I<sub>LIF</sub>) vs ground state energy and deduce temperature from slope



 $\rightarrow$  Great in laminar flames, not applicable in turbulent flames as wavelength scan takes too long



## Laser Induced fluorescence (6)



- Choice of species for LIF thermometry based on Boltzmann distribution
  - Naturally occurring molecules: OH radical, concentration level in typical flames sufficiently high only for T > 1500 K
  - Seeded species:
    - NO, chemically more or less inert, but may not be a good choice for cases studying auto-ignition (NO promotes auto-ignition), caution: NO is toxic
    - Indium, typically via InCI, for example dissolved in liquid fuel such as iso-octane, seeding is difficult in general (compare papers from Hult et al. or Nathan et al.)



## Raman spectroscopy (1)



• Elastic and inelastic light scattering of photons off molecules





## Raman spectroscopy (2)



• Selection rules

 $\Delta J = 0, \pm 2$   $\Delta J = 0 \rightarrow \text{Q-branch}$   $\Delta J = +2 \rightarrow \text{O-branch}$  $\Delta J = -2 \rightarrow S$ -branch

#### Oxygen molecule $O_2$ , T = 1500 K

Simulated "stick spectrum" – infinite resolution

Ro-vibronic Stokes-Raman

Exception: very weak R and P-lines



# Raman spectroscopy (3)



**Experimental setup** Fixed frequency laser filter lens objective Low dispersion Stokes spectrum +5.0e+4 N<sub>2</sub> experiment 1619 K Т - libary background CO2 0.036 libary + bgr O2 0.068 CO 0.042 intensity [a.u.] +5.26+4 0.656  $N_2$ CH<sub>4</sub> 0.025 H<sub>2</sub>O 0.129 H<sub>2</sub> 0.045 Spectrometer н,0 CH H<sub>2</sub> Shuttered CCD +0.0e+0 +5.0e+3 residuum +0.0e+0 -5.0e+3 560 600 640 680 wavelength [nm]



# Raman thermometry (1)



Ratio of  $I_{Stokes}$  to  $I_{anti-Stokes}$ 

Stokes



Spontaneous Raman scattering anti-Stokes



- Typically applied for vibrational levels
- $\rightarrow$  Example N<sub>2</sub>: Temperature sensitivity starting from ~ 500K (otherwise too low fractional population)
- $\rightarrow$  Not very common in combustion community


# Raman thermometry (2)



- Measure entire Raman Stokes spectrum
- Combustion: Typically ro-vibronic spectrum of N<sub>2</sub>
- **High** dispersion  $\rightarrow$  resolve only N<sub>2</sub>, no other molecules

Not very common in combustion research (high dispersion comes along with low signal)

Pure Raman thermometry not common in combustion community



# **Coherent anti-Stokes Raman spectroscopy (1)**



• Non-linear polarization  $P_i = \varepsilon_{i} \chi_{ij}^{(1)} E_j + \chi_{ijk} E_j E_k^{(2)} + \chi_{ijk} E_j E_k E_j + \ldots$ 

- $P_i$ : Polarization
- $E_i$ : Electrical field
- $\chi^{(n)}$ : Susceptibility of n-th order
  - Non-linear effects are observable only at high electrical field strength

≈10<sup>0</sup> ≈ 10<sup>-12</sup> ≈ 10<sup>-23</sup>

➡ Pulsed LASER is prerequisite

In Gases :

$$\chi^{(2)} = 0$$



# **CARS: theoretical background**



• Wave equation describes light emission due to non-linear polarization

$$\nabla^2 \vec{E} - \frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2} = \mu_0 \frac{\partial^2 \vec{P}}{\partial t^2} \quad \text{Here:} \quad P_i = \varepsilon_0 (\chi_{ij}^{(1)} E_j + \chi_{ijkl}^{(3)} E_j E_k E_l)$$

$$\begin{split} \boxed{E_{(\omega_4)} \propto E_{(\omega_1)} E_{(\omega_2)} E_{(\omega_3)} \Big| \chi_{CARS_{(\omega_1,\omega_2,\omega_3)}} \Big|^2 \frac{e^{(i\Delta kl)} - 1}{\Delta k}}{\Delta k} \end{split}$$

Common practice in CARS:  $\omega_1 = \omega_3$ 

$$I_{CARS} \propto I_1^2 I_2 \left| \chi_{CARS_{(\omega_1,\omega_2)}} \right|^2 l^2 \left( \frac{\frac{\sin \frac{\Delta kl}{2}}{2}}{\frac{\Delta kl}{2}} \right)^2$$



#### technische CARS: energy and momentum conservation UNIVERSITÄT DARMSTADT Pump laser Pictorial view of CARS Stokes laser Energy balance: $\omega_3 = 2\omega_1 - \omega_2$ CARS signal (anti-Stokes) Selection rules $\mathcal{O}_1$ 0 $\omega_{2}$ $\omega_{2}$ $\omega_1$ $\omega_3$ $\mathcal{O}_1$ $\omega_{2}$ $\Delta J = 0,\pm 2$ $\Delta v = 1$ $\mathcal{O}_R$ Momentum balance: $k_3 = k_1 + k_1 - k_2$ **Termed phase matching** $k_1$ $k_1$ $\vec{k}_{2}$ $k_3$ $k_{3}$ **Co-linear CARS** BOX CARS: preferred, higher spatial resolution



# **CARS:** phase matching



- Realization of phase matching
  - Pump laser: 532 nm (frequency-doubled Nd:YAG)
  - Stokes laser: 607 nm (broadband dye laser)
  - CARS signal: 473 nm





## **CARS:** broad band and scanning







## **CARS:** thermometry



• Typical application in turbulent flames: ro-vibronic N<sub>2</sub>-broad band CARS



Temperature obtained by fitting CARS spectrum to experimental spectrum

Temperature information is contained in line-strength~ $N_i^2$  (in  $\chi^3$ -tensor)

Based on Boltzmann distribution

$$\frac{N_i}{\sum_i N_i} = \frac{g_i e^{-E_i/kT}}{\sum_i g_i e^{-E_i/kT}}$$



## CARS: single shot spectra and spectral fit







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# CARS: experimental setup, combined with CO-LIF





# CARS: pro and con



Advantages:

- precise single-shot temperature measurement of gas phase
- coherent signal allows detector placed far away from combustor
- No calibration required

Disadvantages:

- complicated optical setup
- spatial resolution in mean beam propagation direction only ~0.5mm, often worse
- mostly point-measurements (new fs/ps CARS allows for 1D and 2D CARS!!)



# **Spectroscopic methods – classification**



#### Based on

• Boltzmann distribution

$$\frac{N_i}{N} = \frac{g_i \exp(-E_i / kT)}{\sum_j g_j \exp(-E_j / kT)} = \text{unique function of } T$$
  
 $g_i$ : degeneracy factor  $E_i$ : energy quantum state; both from quantum mechanics

- Temperature-dependent absorption/emission
- Density measurements via equation of state

$$pV = NkT \rightarrow T = \frac{pV}{Nk}$$



# **Temperature dependent emission/absorption**



- Fluorescence tracer added to gas
  - Typical tracers
    - Hydrocarbons: aromates, ketones or aldehydes
    - Atoms
- Pro
  - Tracer and its spectroscopic characteristics can be chosen in dependence of measuring task
- Con
  - Hydrocarbon tracer is thermally decomposed for T > ~700 K, not applicable in flames, but for example compression stroke in IC engine
  - Tracer may influence chemical and physical properties of the fluid
  - Spectroscopic properties of tracer often not independent of surrounding gas phase



# **Typical tracers for LIF thermometry**



- Ketones:
  - acetone
  - 3-pentanone <sub>H<sub>3</sub>C CH<sub>3</sub></sub>
- Aromates: toluene

- Aldehydes: acetaldehyde  $_{H_3C} \xrightarrow{\parallel}_{H}$
- List is not complete: search for LIF-tracers with higher quantum yield, less O<sub>2</sub>-quenching, etc. goes on

 $CH_3$ 



# **Classification of LIF-thermometry**



- Two options
  - Two line excitation one color detection: excite tracer at two different wavelengths (two lines) and measure fluorescence broadband (one color)
  - $\rightarrow$  Exploit temperature dependent **absorption** band
  - Single line excitation two color detection: excite tracer at one wavelength (single line) and measure fluorescence at two spectrally separated bands (two color)
  - $\rightarrow$  Exploit temperature dependent emission band



# **3-pentanone LIF thermometry**



• 3-pentanone: Example for **two line – one color** thermometry



- Spectra are normalized
- total integral increases with temperature
- Two lasers/two cameras needed
- For more information see Schulz, Dreizler, Ebert, Wolfrum Combustion Diagnostics, Springer Verlag 2007

$$\frac{S_1(\lambda_1, \boldsymbol{\rho}, \boldsymbol{T})/I_{\text{Laser}_1}(\lambda_1)}{S_2(\lambda_2, \boldsymbol{\rho}, \boldsymbol{T})/I_{\text{Laser}_2}(\lambda_2)} \frac{\pi_2}{\pi_1} = \frac{\sigma_1(\lambda_1, \boldsymbol{T})}{\sigma_2(\lambda_2, \boldsymbol{T})} \frac{\phi_1(\lambda_1, \boldsymbol{T})}{\phi_2(\lambda_2, \boldsymbol{T})} = \boldsymbol{F}(\boldsymbol{T})$$



# **Toluene LIF thermometry**



• Toluene: Example for **single line – two color** thermometry



- Spectra are normalized
- Strong quenching by O<sub>2</sub> → reducing high quantum yield compared to oxygen-free atmosphere
- For more information see Peterson, Baum, Böhm, Dreizler, Appl. Phys. B 2014

Application example follows at end of this chapter



# **Spectroscopic methods – classification**



#### • Based on

• Boltzmann distribution

$$\frac{N_i}{N} = \frac{g_i \exp(-E_i / kT)}{\sum_j g_j \exp(-E_j / kT)} = \text{unique function of } T$$
  
 $g_i$ : degeneracy factor  $E_i$ : energy quantum state; both from quantum mechanics

- Temperature-dependent absorption/emission
- Density measurements via equation of state

$$pV = NkT \rightarrow T = \frac{pV}{Nk}$$



# Rayleigh spectroscopy – in combination with Raman if gas composition unknown



Elastic and inelastic light scattering of photons off molecules





## Rayleigh thermometry: known gas comp.



Rayleigh signal intensity 
$$F_{ray}(x) = C_{calib} \sigma_{ray} I_{laser}(x) N/V$$

- With known Rayleigh cross-section σ<sub>ray</sub>(known gas mixture, no reactions), measured laser intensity, and calibration Ray-signal proportional to local gas density
- Deduce temperature in combination with equation-of-state
- Example: ideal gas law pV = NkT

$$\rightarrow T = \frac{pV}{Nk} = \frac{p \cdot C_{calib} \cdot \sigma_{Ray} \cdot I_{laser}(x)}{k \cdot F_{Ray}(x)}$$

• Wavelength-dependent Ray cross section of gas *i* can be calculated from index of refraction  $4\pi^2(n-1)^2$ 

$$\sigma_{ray,i} \cong \frac{4\pi^2 \left(n_i - 1\right)^2}{\left(N_A / V\right)^2 \lambda^4}$$





# Rayleigh thermometry: <u>unknown</u> gas comp.



- Rayleigh signal intensity  $F_{ray}(x) = C_{calib} \sigma_{ray} I_{laser}(x) \frac{N}{V}$
- Measure laser intensity and perform calibration Ray-signal proportional to local gas density
- Gas mixture unknown (for example due to chem. reactions or mixing)
  - $\rightarrow$  gas composition must be measured
  - $\rightarrow$  simultaneous Raman scattering
- Once gas composition is known, effective Rayleigh cross-section can be calculated by:

$$\sigma_{ray} = \sum_{i} X_{i} \sigma_{ray,i}$$



# Raman/Rayleigh spectroscopy (1)



- Measure entire Raman Stokes spectrum
- Low dispersion → measure multi-scalars and deduce temperature either from Rayleigh scattering (see below) or from absolute gas density
- Multi-scalar: exploit different energy separation between quantum states for different molecules





## Raman/Rayleigh spectroscopy (2)

- Measure entire Raman Stokes spectrum with **low** dispersion
- Ram in combination with Ray common for studying details of **open flames** but Ram used then for conc. measurements
- Ram for thermometry via gas density used in confined flames in combination with conc. measurements







# Simultaneous Raman/Rayleigh spectroscopy



• Raman scattering  $\rightarrow$  species concentrations  $N_i(r)$ 

$$S_{ram,i}(\vec{r}) \propto \sigma_{ram,i}(\vec{r}) I_{Laser} N(\vec{r})$$

• Rayleigh scattering  $\rightarrow$  density, with EOS  $\rightarrow$  temperature T(r)

$$S_{ray}\left(\vec{r}\right) \propto \sigma_{ray}\left(N_{i}\left(\vec{r}\right)\right) I_{Laser}\sum N_{i}\left(\vec{r}\right)$$

$$\sigma_{ray} = \sum_{i} \left(\frac{N_{i}\left(\vec{r}\right)}{\sum_{j}N_{j}\left(\vec{r}\right)}\right) \sigma_{ray,i} \quad \overrightarrow{\text{Ideal gas law}} \quad \overrightarrow{T\left(\vec{r}\right)} \propto \frac{1}{\sum N_{i}\left(\vec{r}\right)}$$
(EOS)

Iterative procedure to determine temperature and species

See chapter 7 Gas Concentration Measurements



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#### **Motivation**

- Gas temperature is a leading parameter in combustion
- Internal combustion engines
  - Temperature dependencies
    - Mixture preparation
    - Ignition, auto-ignition
    - Combustion
    - Pollutant formation
    - Heat loss

- Measure and understand spatial and temporal evolution of unburned gas temperature in IC engine
- For details see: Peterson et al. PCI 2013







# **Temperature Fields in IC Engines**



- Laser Induced Fluorescence (LIF) Thermometry
- Toluene LIF Thermometry
  - Single line excitation
    - 248 or 266 nm
  - Single or two color detection
- IC Engines
  - Temperature stratification<sup>1,2,3,4</sup>
  - Low repetition rates
- Focus here
  - High-speed toluene LIF and PIV measurements
  - Temporal evolution of 2D temperature field





# **Experimental Setup**



- High-speed imaging
  - 2D PIV
    - <sup>Red Image</sup>
       532 nm (Nd:YVO<sub>4</sub>)
    - HS CMOS
  - Toluene LIF
    - 266 nm (Nd:YAG)
      - 1 mJ at 6 kHz
    - HS-IRO CMOS
- Laser sheets centralized in tumble plane
- Image through quartz glass cylinder
  - T-LIF independent:
    - Absorption
    - Laser fluence
    - Mixture inhomogeneities



Blue Image





# **Experimental Setup**

Toluene LIF







**Bandpass filters** 

B: 350 nm SP C: Beam Splitter

D: 300 nm SP

A: 275 nm LP (x2)

• HR 250-300 nm







# **Experimental Setup**

- Field-of-view
  - 25x30 mm<sup>2</sup> region
  - Offset from cylinder axis
  - Near cylinder head
  - Cylinder head
    - Set temperature: 333K
    - Expected thermal gradients near colder surfaces
- Images
  - 3x3 median filter
  - 3x3 pixel binning
  - Spatial resolution
    - 0.08 mm/pixel









#### **Engine Operating Conditions** DARMSTADT 1000 RPM $N_2$ + toluene Intake Exhaust (premixed 1m) Intake Nitrogen Toluene vapor (2.5% vol.) 95 kPa, 295K Motored Operation (72 cycles) ■ CR = 8.5 LIF signal dynamic range -Polytropic Temperature -- Pressure - LIF Signal - Polytropic Temperature Κ Temperature (K) Pressure (bar) LIF Signal Temperature CAD CAD

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# LIF Signal

- Calibration (LIF  $\rightarrow$  Temp)
  - LIF ratio (72 cycles)
    - 5x5 mm<sup>2</sup> region
  - Calibrate to polytropic temperature
- Precision Uncertainty
  - $LIF_{ratio, stdev} / LIF_{ratio}$
  - Pixel-wise (0.08 x 0.08 mm<sup>2</sup> region)
  - LIF precision uncertainty
    - T = 295 ± 5 K (2%)
    - T = 540 ± 29 K (5.2%)
  - 10x10 pixel region
    - T = 540 ± 19K (3.5%)







# **Temperature Images for fired operation**



- Compression
  - Homogeneous temperature distribution
  - Temperature "structures" not present



- Cold temperatures emerge from cylinder head
- Out-gassing of crevice gases
- Cold gas entrainment from right side
  - 50 K colder





# **Temperature distributions**



- Compression
  - Homogeneous temperature distribution
  - Gaussian-like distribution
- Expansion
  - Temperature inhomogeneities
  - Skew / bimodal distributions



PDF



# **Temperature Distribution**

- Identifying temperature inhomogeneities
  - Cold gas
- Gaussian fit to bulk gas temperature
- Subtract from temperature distribution
  - Cold gas distribution
- Cold temperature inhomogeneities
  - < peak of cold gas distribution</pre>









# **2D PDF Cold Temperature**

- 72 motored cycles
- Location, occurrence of cold temperature
- Compression
  - Colder temperatures near cylinder head
  - Low probability (< 30%)</li>
  - Temperature boundary layer not visible
- Expansion
  - Cold regions near cylinder head
  - Cold gas enters viewing plane from crevices



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Temperature and velocity field

— cold temperature threshold



# High speed toluene PLIF combined with PIV



Visualization of outgassing from crevices



Peterson et al. Proc. Combust. Inst. 34, 3653-3660 (2013)


## Conclusions temperature/velocity measurements in IC engine



- High-speed Toluene-LIF and PIV to assess thermal transport in IC engine
- 2-color detection
  - LIF independent from absorption and local mixing
  - Precision uncertainty limited to 3-6% (dependent on temperature)
- Compression
  - Quasi-homogeneous temperature distribution
- Expansion
  - Evident colder gas evolution
  - Thermal stratification
- Cold front tracking
  - LIF vs. PIV
  - Transport of cold gas
  - Discrepancies
    - Out-of-plane motion



## **Overall summary**



- Spectroscopic methods well suited for minimal invasive thermometry
- High resolution in time and reasonable resolution in space
- There is not the single method best suited for all tasks choice depends on measurement task
- Optical access required can be a problem
- High instrumental effort and expert knowledge needed

