

Chapter 8: High-speed Laser Combustion Diagnostics – General Aspects

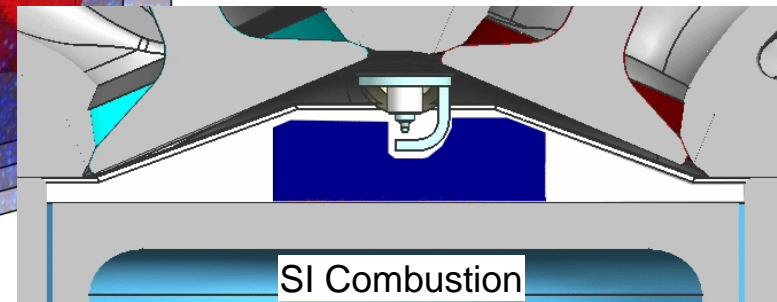
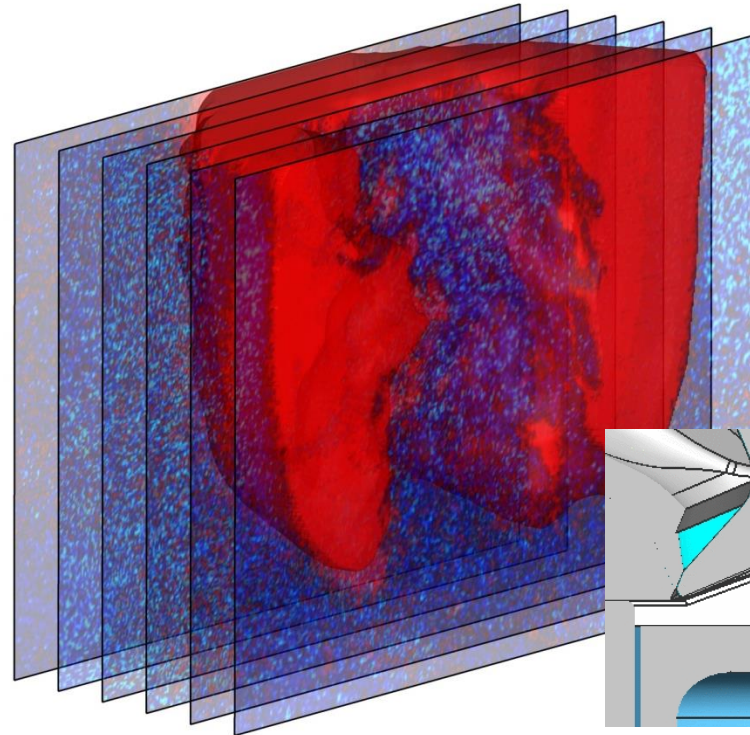


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TU Darmstadt, Germany
Mechanical Engineering – Reactive Flows and Diagnostics



A. Dreizler



SI Combustion

Photron.com

Contents



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- Why high-speed laser diagnostics?
- Instrumentation
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State-of-the-art laser combustion diagnostics

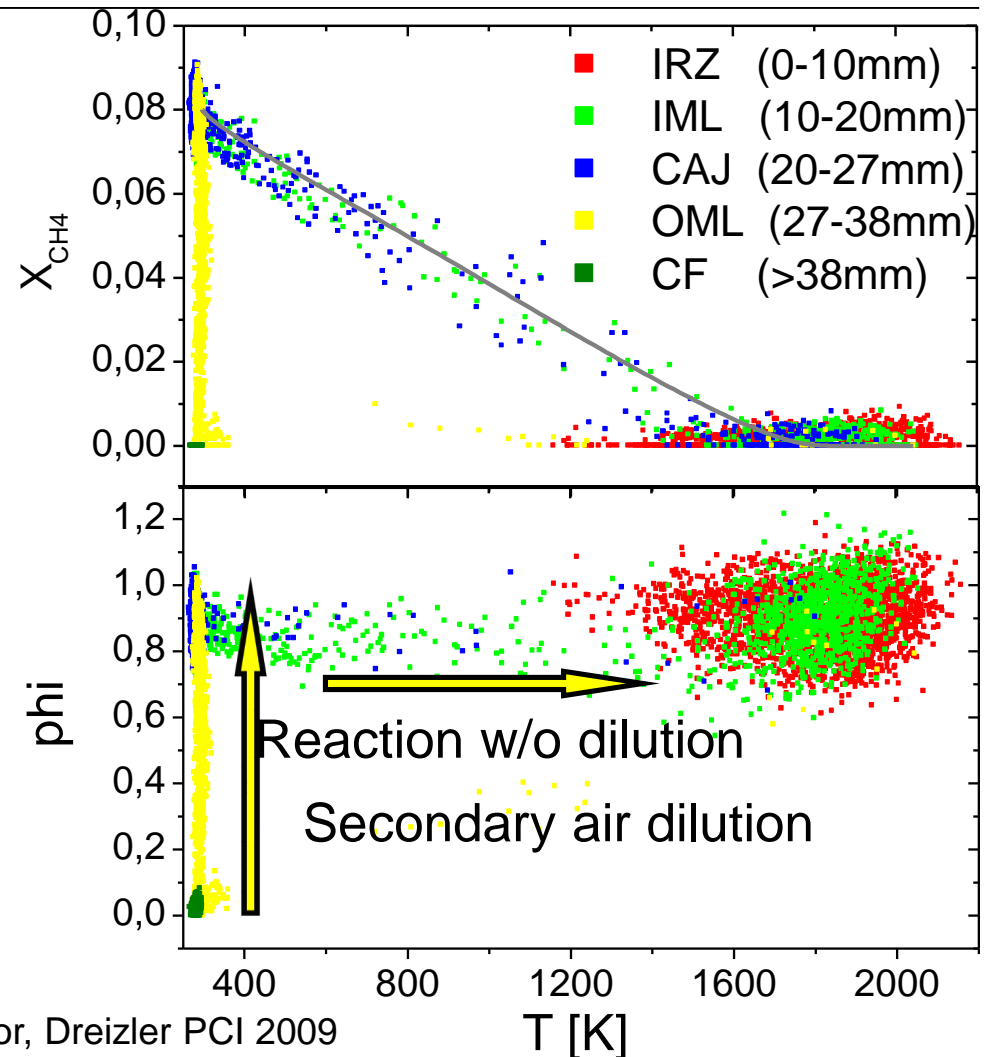
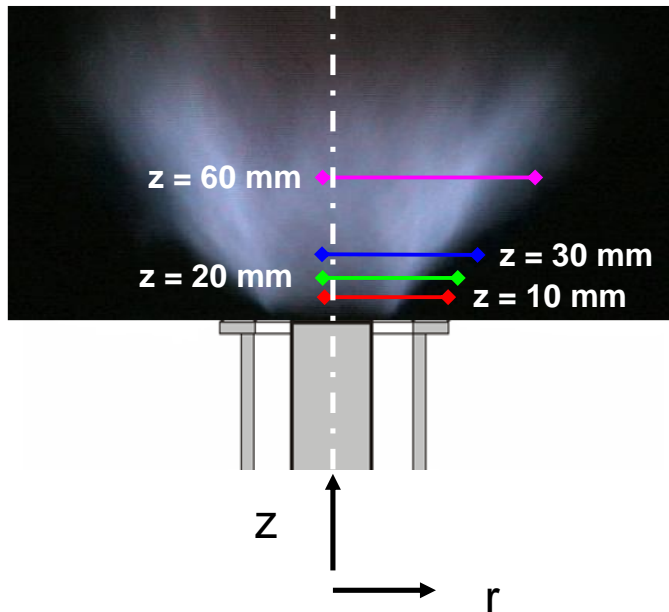


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- Flow and multi-scalar measurements
 - Low sampling rates (<100 Hz)
 - High precision and accuracy
 - Good for measuring statistical moments (single-point, two-point statistics)
 - Example: scatter plots by multi-scalar Raman/Rayleigh spectroscopy

State-of-the-art laser combustion diagnostics

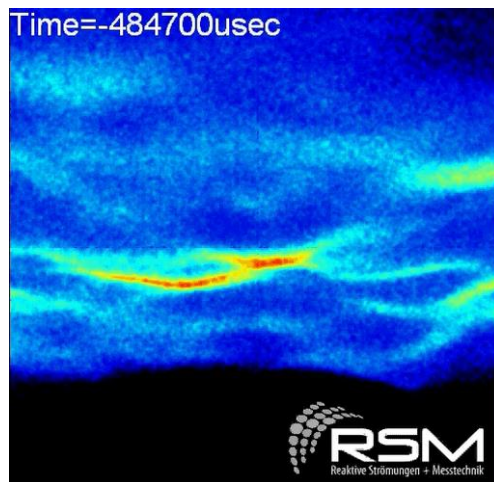
- Example: scatter plots by multi-scalar Raman/Rayleigh spectroscopy, lean premixed swirl flame



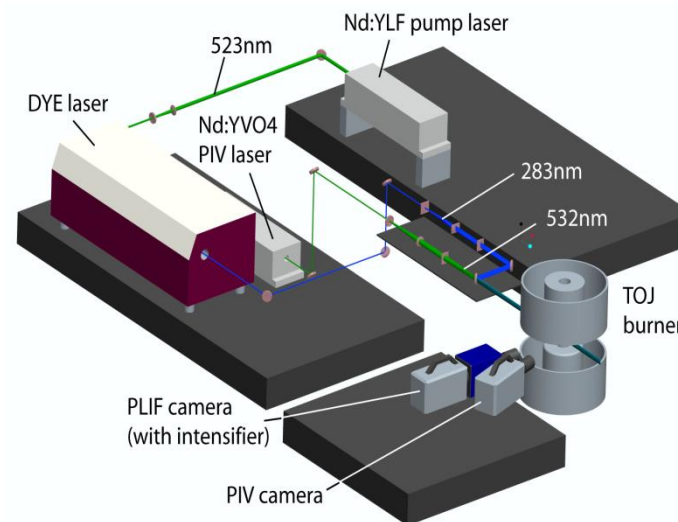
Gregor, Dreizler PCI 2009

Motivation for high speed diagnostics

- Example flame extinction (w/o subsequent re-ignition)
 - Here turbulent opposed jet flows, partially premixed flame
 - Bulk flow rates close to global extinction

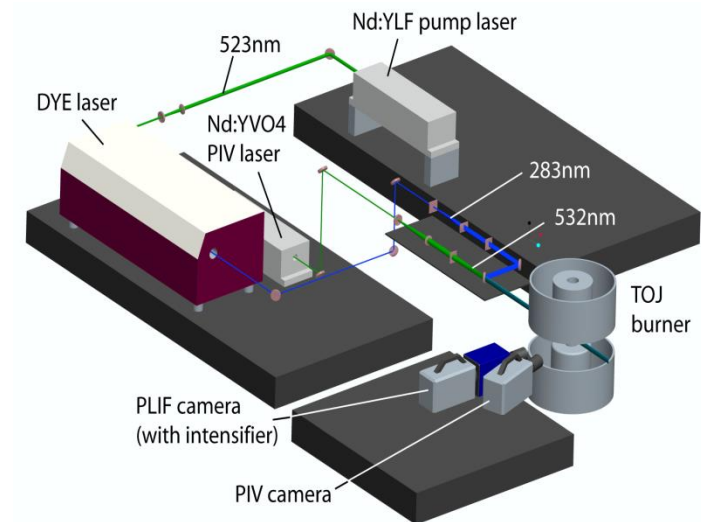
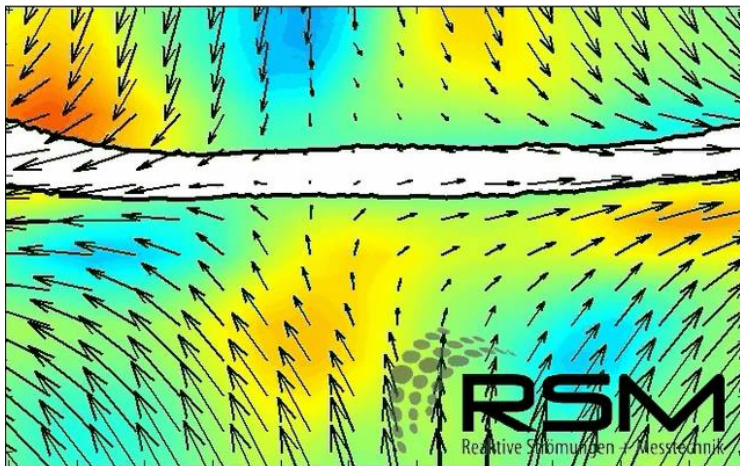


Böhm, Dreizler PCI 2009



Motivation for high speed diagnostics

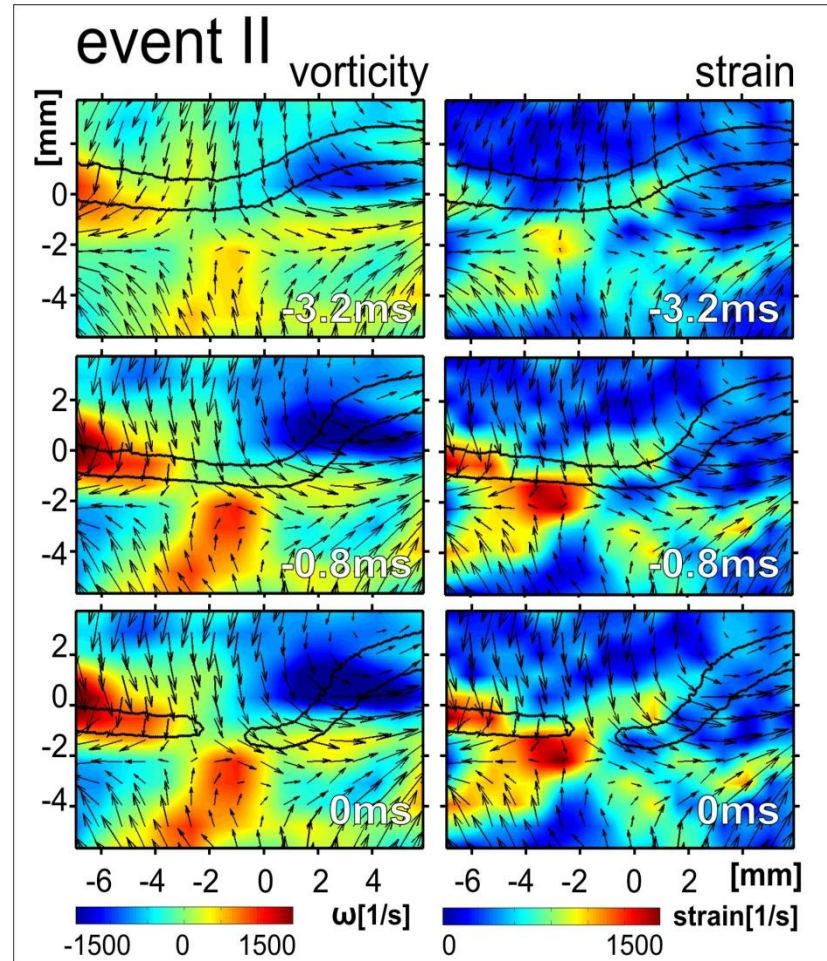
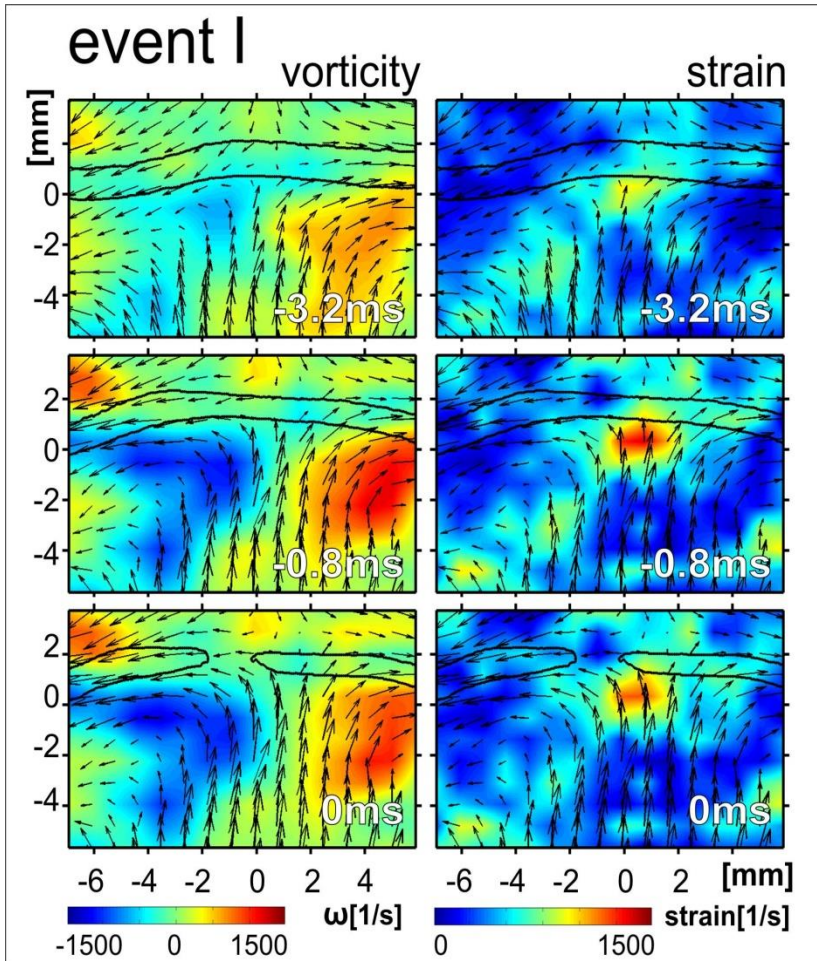
- Example flame extinction (w/o subsequent re-ignition)
 - Here turbulent opposed jet flows, partially premixed flame
 - Bulk flow rates close to global extinction



Böhm, Dreizler PCI 2009

→ **Tracking extinction needs high sampling rates, post event-triggering and sequence lengths over 10 – 100ms**

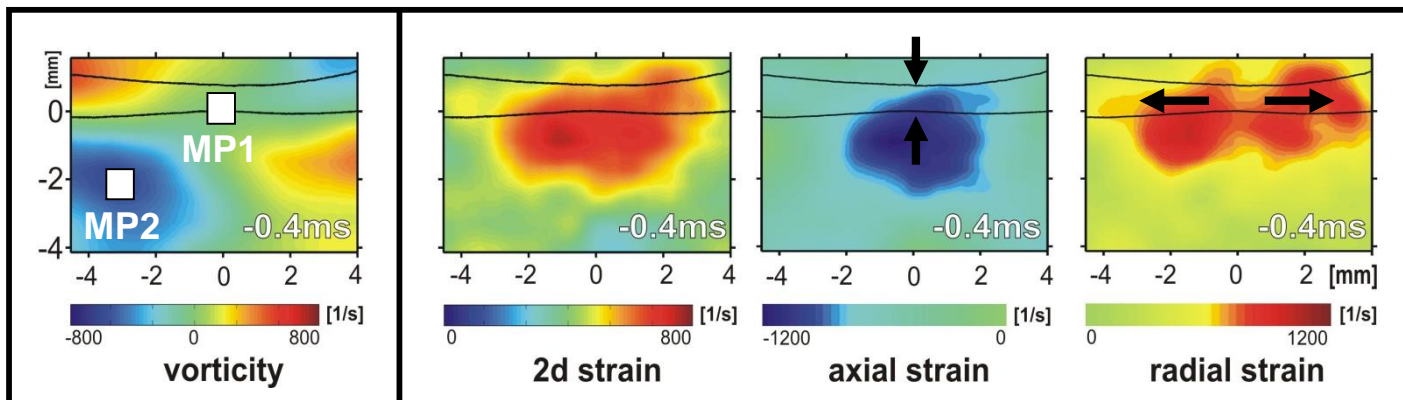
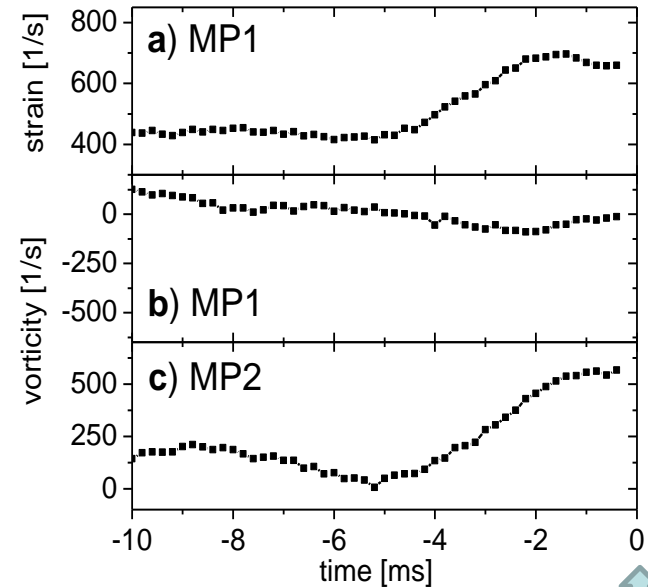
Individual extinction events



→ multiple vortices act coherently generating regions of high strain close to the flame at the onset of extinction

Conditional averages

- Maximum of axial strain surrounded by maxima of radial strain
- Imposed strain requires time to cause extinction
- Time history is important
- Diffusion requires time to reduce scalar gradients



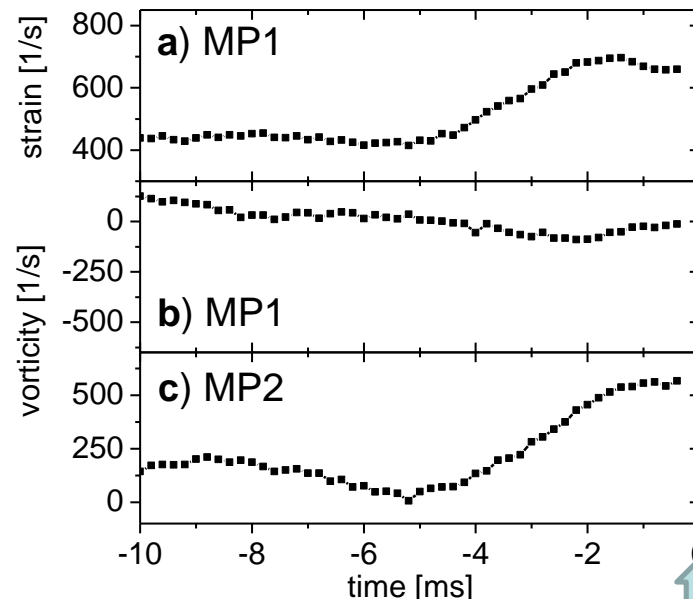
↑
extinction

Multi-parameter diagnostics at high speed

- Simultaneous measurement of velocity fields and qualitative scalar fields that mark features of flames (such as flame fronts) allows determination of conditional velocities:
 - Switch from lab-coordinates to flame-fixed coordinates
 - De-convolute effects from intermittency
 - Better observation of interaction between flow and scalar fields

- Conditional strain

- Conditional vorticity





- Phenomena requiring high speed diagnostics for better understanding
 - Extinction and re-ignition
 - Flame stabilization of lifted flames and flame propagation
 - Flashback in nozzles
 - Auto- and spark-ignition
 - Cycle-to-cycle variations in IC engines
 - 4D-imaging

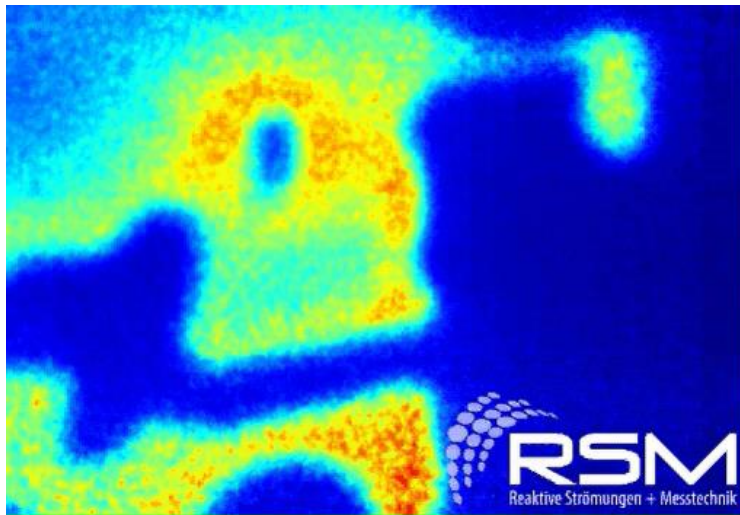
- What repetition rate is needed?

Typical time scales – lab-scale turbulent premixed flame

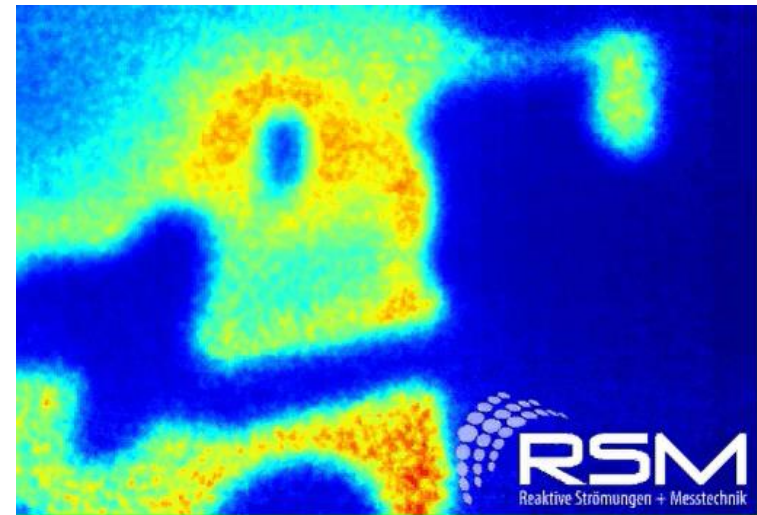
- $T_{\text{int}} \sim 1.0\text{ms} \rightarrow$ Sampling rate ($0.1 \times T_{\text{int}}$) $\sim 100\mu\text{s} \rightarrow 10\text{ kHz}$

OH PLIF @ 5 kHz

@ 10 kHz



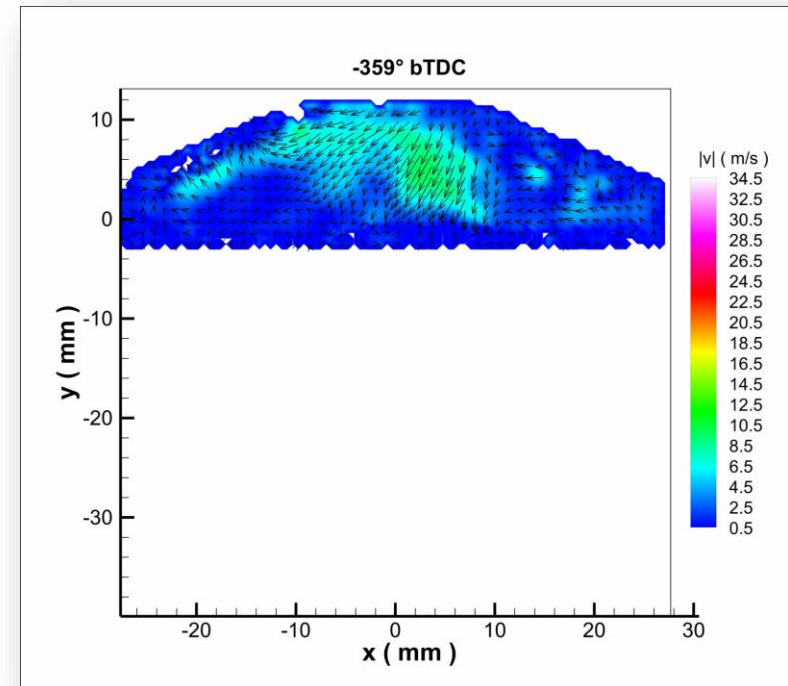
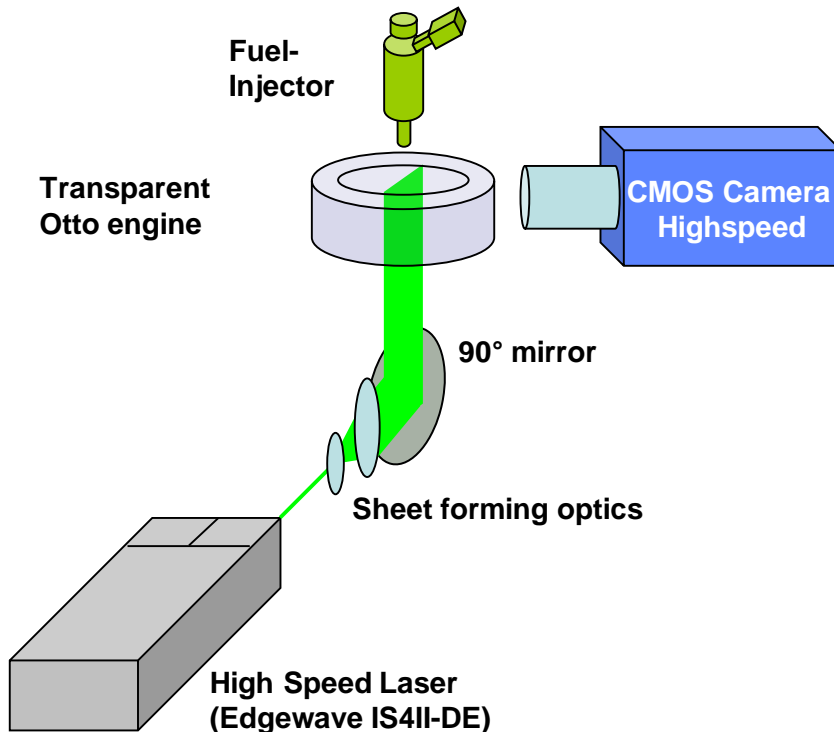
sequence “judders”



sequence runs “smoothly”

Typical time scales – IC engine

- IC engine operating at 1000 rpm → resolving 1 °CA corresponds to 166 μs → 6 kHz



Flow field during compression
@ 6 kHz 2C-PIV;

E. Baum, et al. *Flow Turbulence Combust.* 92, 269-297 (2014)

Statistically correlated measurements: Scales to be resolved – integral time scale (T_{int})

- Swirling annular flow: non-reacting and premixed flame (lab scale)

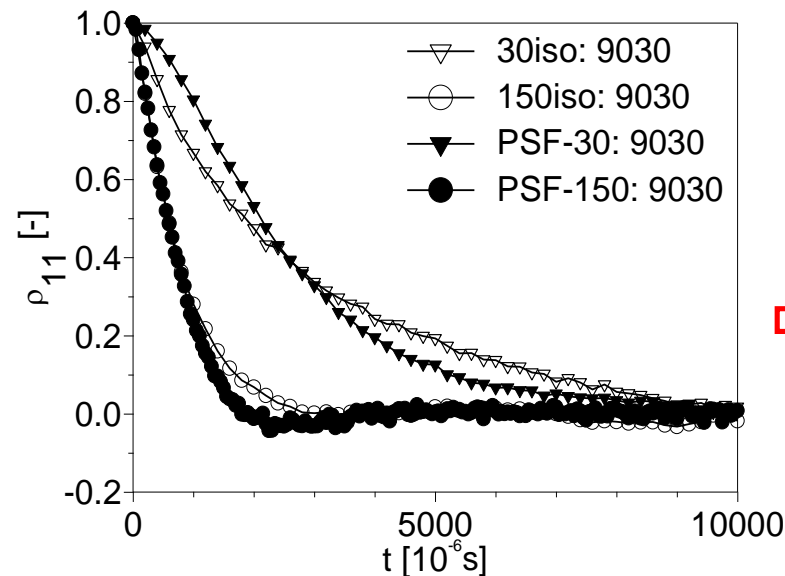


Iso-pressure surface
Janicka et al. 2007

LDV time-series →

$Re = 10,000 - 40,000$

$P_{th} = 30 - 150 \text{ kW}$



→ $T_{int} \sim 1.0 \text{ ms}$
($Re=10,000$)

Schneider et al.
FTaC 2005

Statistically correlated measurements: Scales to be resolved – integral time scale (T_{int})



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- Swirling annular flow: non-reacting and premixed flame (lab scale)



Iso-pressure surface
Janicka et al. 2007

$$Re = 10,000 - 40,000$$

$$P_{th} = 30 - 150 \text{ kW}$$

Nyquist-Shannon theorem $f_{\text{repetition rate}} \geq \frac{2}{T_{int}} = 2000 \text{ fps}$

Scales to be resolved – Kolmogorov time scale

- Kolmogorov time scale τ_K (integral length scale L_{int} from 2-point correlations)

$$\tau_K = \left(\frac{\nu}{\varepsilon} \right)^{0.5} ; \quad \varepsilon = \frac{k^{1.5}}{L_{\text{int}}} \quad \begin{array}{l} \text{Example} \\ \text{Swirl flame} \\ \text{Re} = 40,000/10,000 \end{array} \quad \tau_K \sim 100 \mu\text{s (representative estimate)}$$

- Nyquist-Shannon theorem

$$f_{\text{frame rate}} \geq \frac{2}{\tau_K} \quad \longrightarrow \quad f_{\text{frame rate}} \geq 20000 \text{ fps}$$

Imaging:
Fulfilled by state-of-the art
CMOS camera technology

Interdependency of time and length scales

Pixel rate Temporal resolution

- Field of View: $l_{\text{FOV}} = n_x \cdot \Delta x = n_x \cdot l_{\text{px}} \cdot M$
- Nyquist-Shannon: $l_{\text{limit}} \geq 2 \cdot \Delta x$

$$\frac{l_{\text{FOV}}}{l_{\text{limit}}} = \frac{1}{2} \sqrt{\frac{R_{\text{px}} \cdot \tau_{\text{limit}}}{2}}$$

Spatial dynamic range

Laser sheet

Spatial and temporal resolution are interconnected via the maximum pixel rate R_{px} (read-out-rate of CMOS)

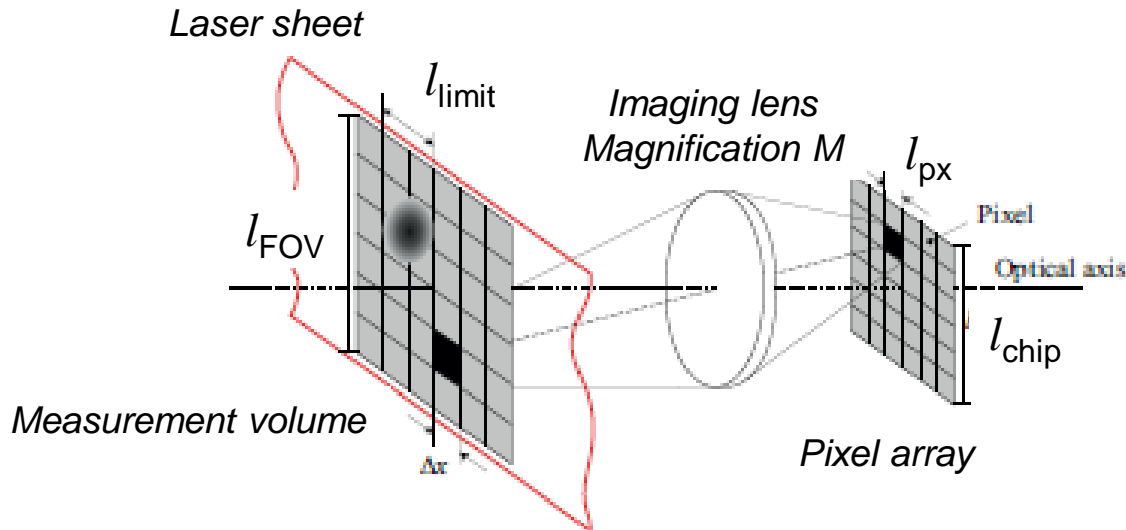
Measurement volume

Δx

Pixel array

Interdependency of time and length scales

$$\left. \begin{array}{l} R_{\text{px}} = 20 \cdot 10^9 \text{ px/s} \\ \text{Magnification} = 1 \\ \tau_{\text{limit}} = \tau_K = 100 \mu\text{s} \\ l_{\text{FOV}} = 20 \text{ mm} \end{array} \right\} \underbrace{\frac{l_{\text{FOV}}}{l_{\text{limit}}} = 500}_{\text{Spatial dynamic range}} \Rightarrow l_{\text{limit}} = 40 \mu\text{m}$$



Interdependency of time and length scales

$$R_{\text{px}} = 20 \cdot 10^9 \text{ px/s}$$

$$\text{Magnification} = 1$$

$$\tau_{\text{limit}} = \tau_K = 100 \mu\text{s}$$

$$l_{\text{FOV}} = 20 \text{ mm}$$

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Spatial dynamic range

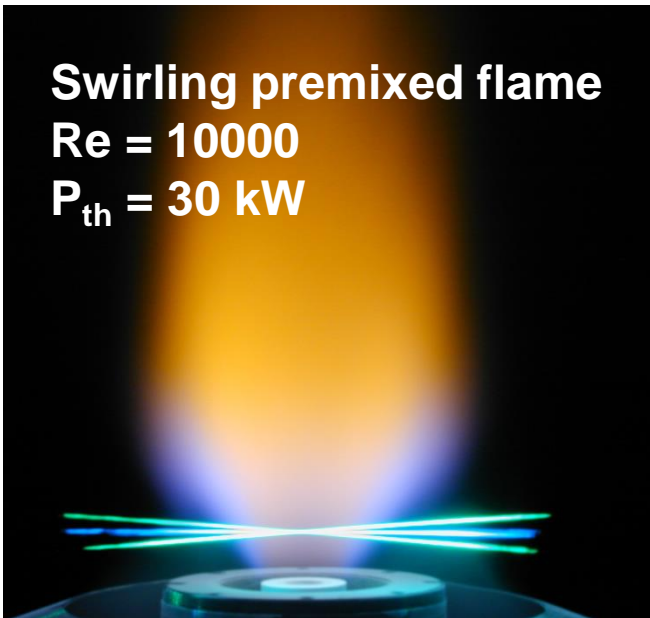
$$l_K = \left(\frac{v^3}{\varepsilon} \right)^{0.25} \Rightarrow l_K = 50 \mu\text{m}$$

Same range

Swirling premixed flame

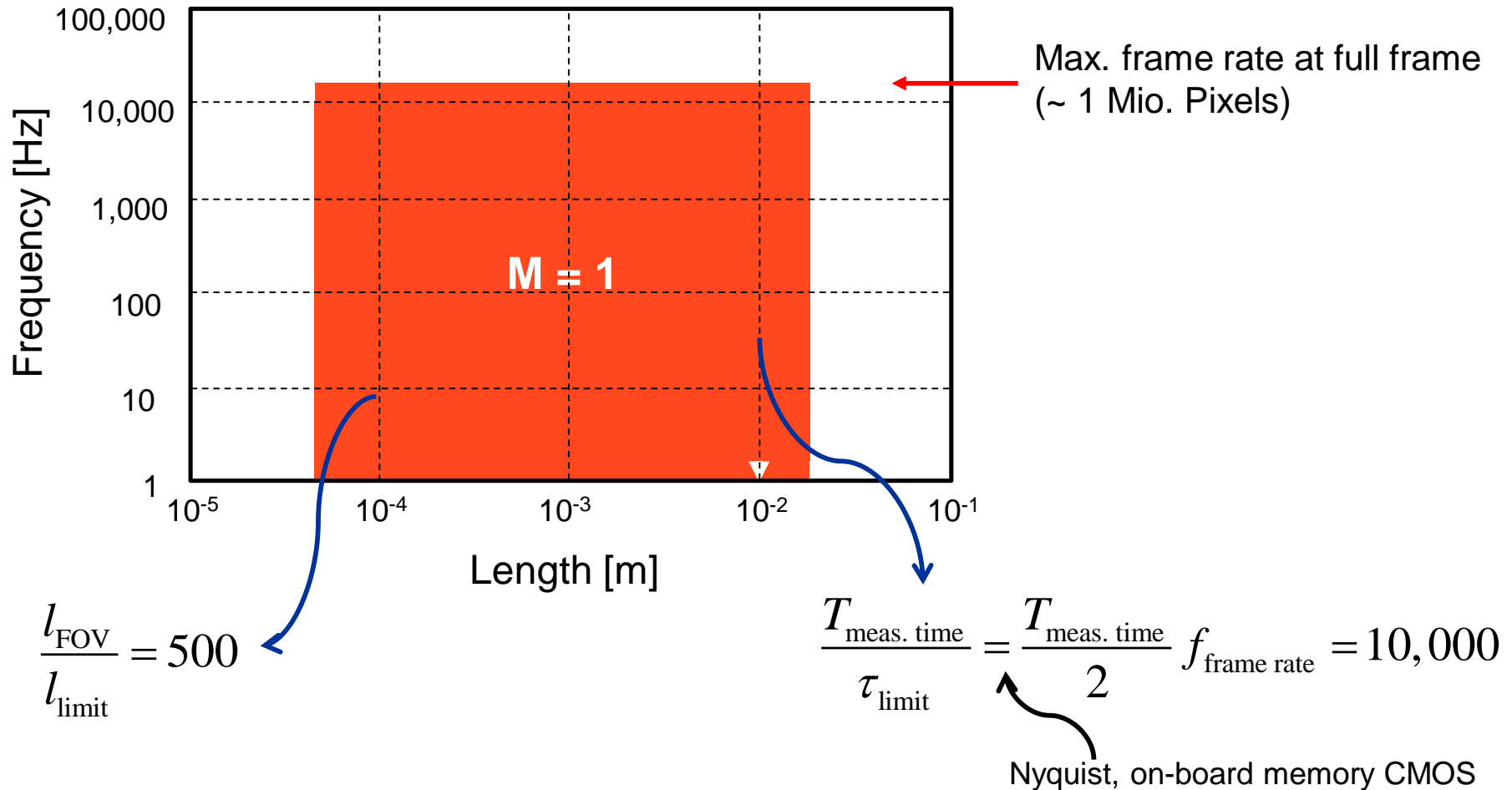
Re = 10000

P_{th} = 30 kW

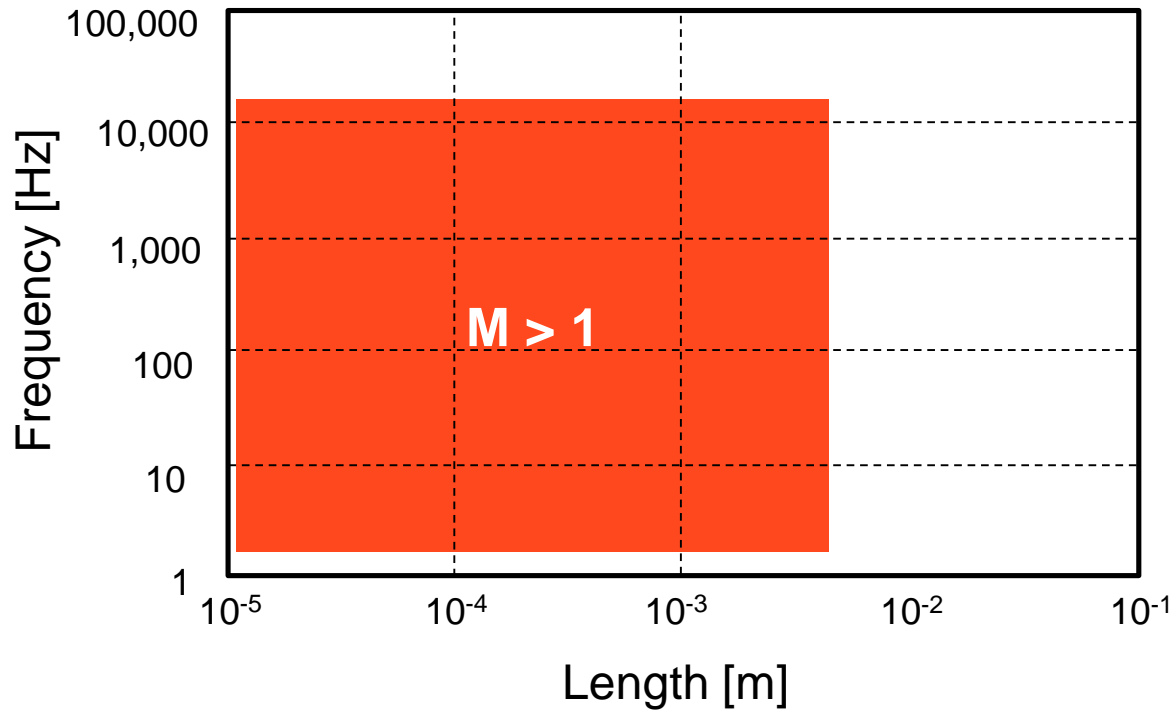


Lab flames, present CMOS technology:
Kolmogorov length and time scales resolvable
FOV contains 2-5 integral length scales

Dynamic ranges – spatial and temporal



Dynamic ranges – spatial and temporal



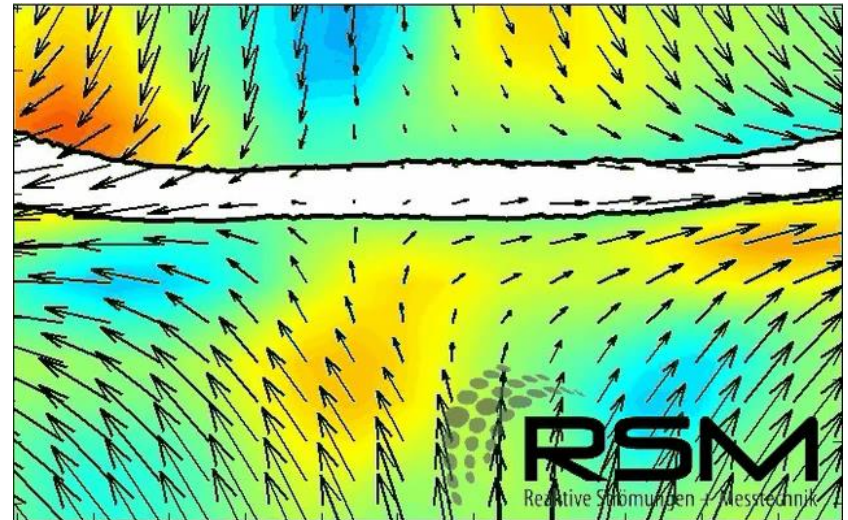


- Field of application
 - Experiments where only few realizations or short measurement periods are available (shock tubes, IC engines, ...)
 - Transients in combustion
 - ignition, extinction
 - blow off, flashback
 - flame propagation, cyclic variations ...
- Instrumentation specific to spectral range and diagnostic method
 - Towards 4D imaging (3D in space + time) → new high speed lasers and CMOS cameras

(conditional) statistics

Ex2: High speed imaging

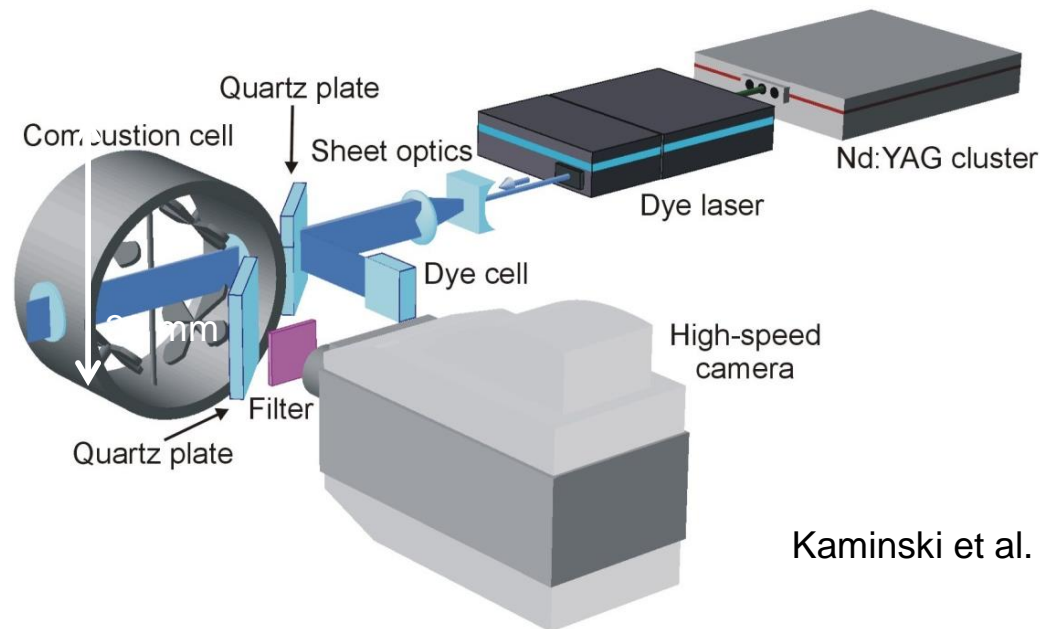
- Rapid progress of laser and camera technology over the last 6-8 years
- Recent reviews on high speed imaging
 - Böhm et al. (FTaC 2011)
 - Thurow et al. (MST 2013)
 - Sick (PCI 2013)
- Requirements
 - High power lasers
 - High frame rate cameras



Extinction in turbulent opposed jet flame
B. Böhm et al. PCI 2009

Burst lasers for high speed imaging

- Low duty cycle, high pulse energies
 - Aldén group (Lund)
 - Cluster of 4 Nd:YAG lasers, frequency doubled
 - 4 – 8 pulses/burst, <500mJ/pulse
 - Use of harmonics directly or for pumping a dye laser/dye laser cluster



Kaminski et al. PCI 2000

Burst lasers for high speed imaging



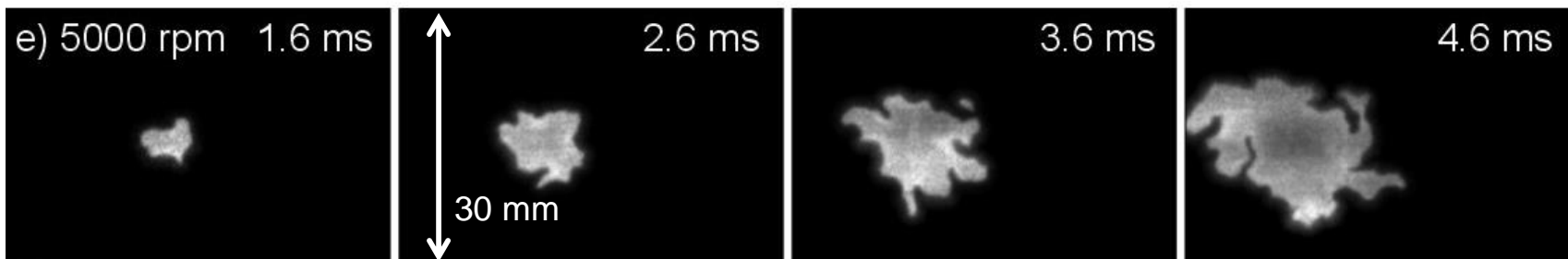
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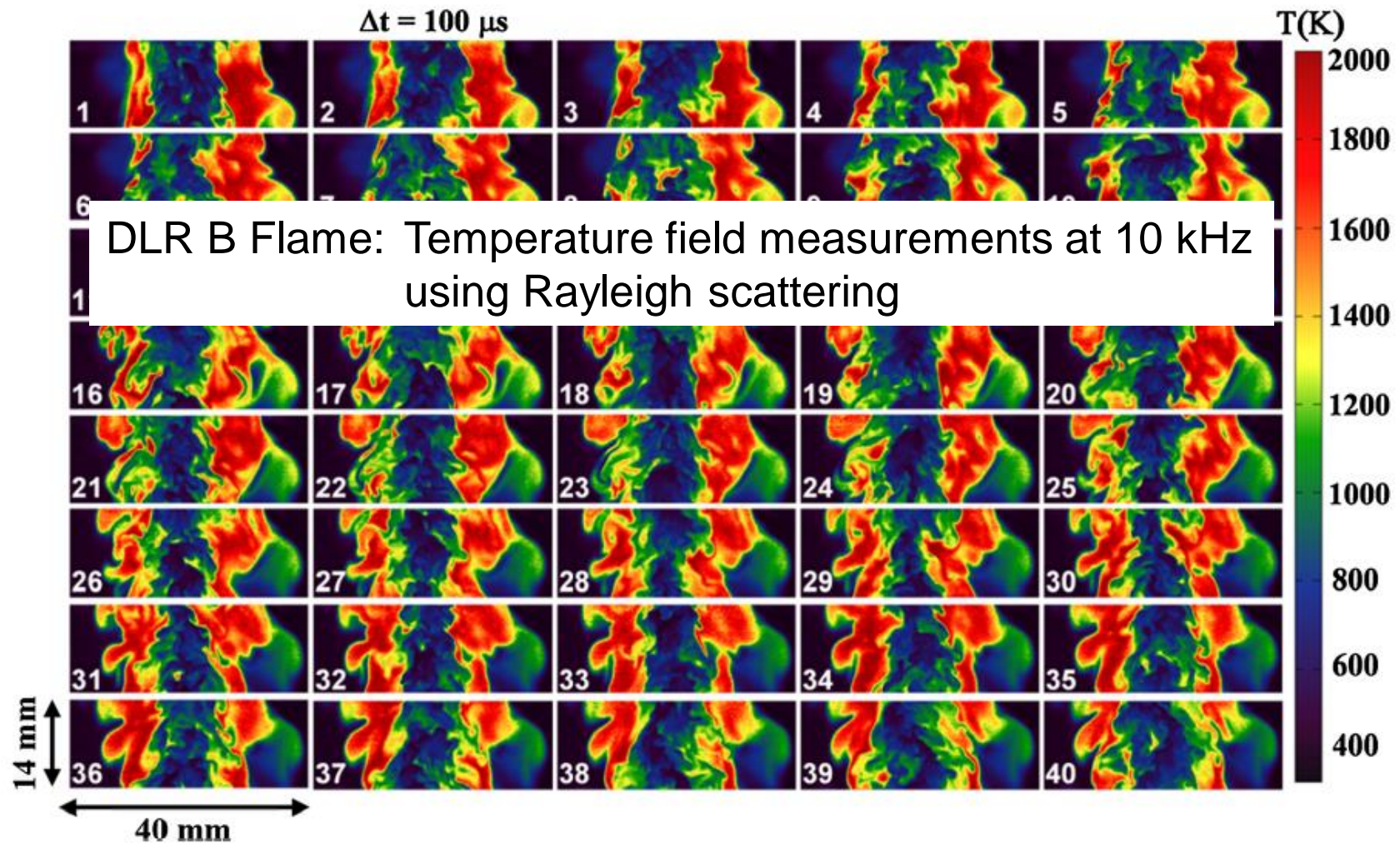
LUND
UNIVERSITY

OH-PLIF, $\Delta t = 1 \text{ ms}$



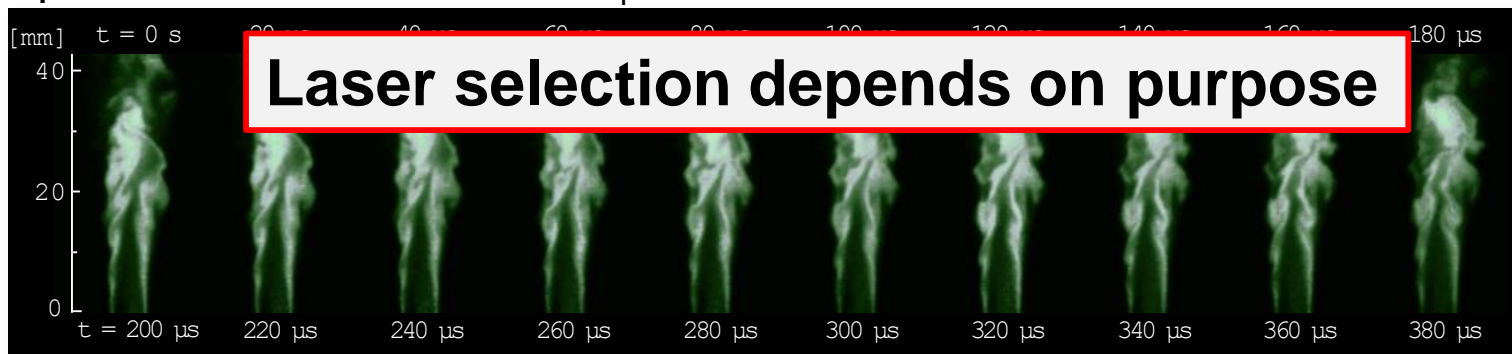
Turbulent flame kernel propagation following spark ignition, stoich. CH_4/air

Burst lasers for high speed imaging



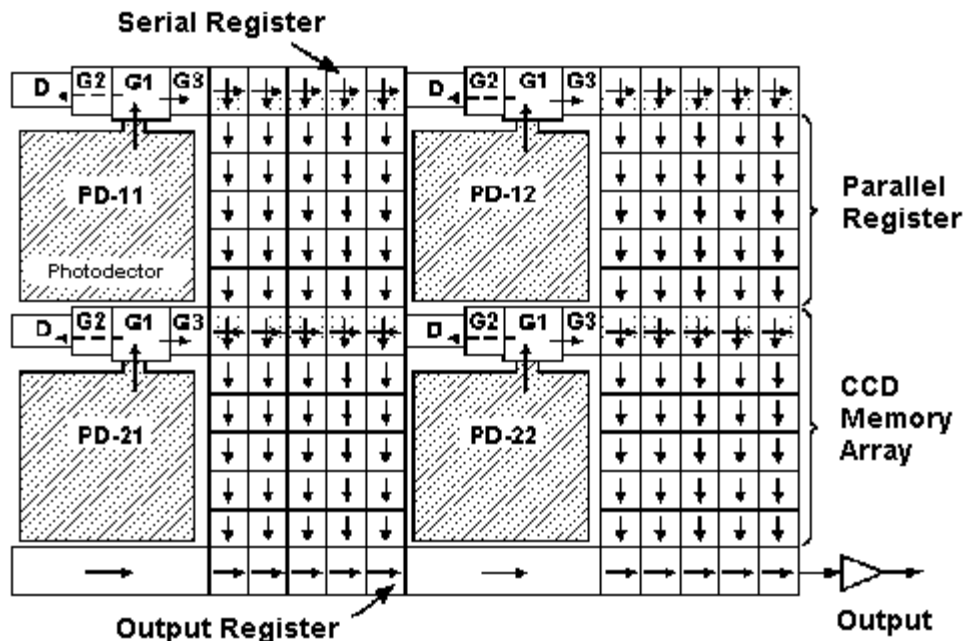
Continuously pulsed high speed lasers

- High duty cycle, low pulse energies
 - Long pulse-lasers: $\Delta t_{\text{laser}} > 100\text{ns}$ → intra-cavity conversion for VIS, UV generation
 - Short pulse-lasers: $\Delta t_{\text{laser}} < 20\text{ns}$ → extra-cavity conversion for VIS, UV generation
 - Suitable to pump dye lasers
 - Most recent specifications:
 - 50 kHz, 200 W pump power @ 532 nm → 7 W @ 283nm (2-step SHG)
S. Hammack, C. Carter, C. Wünsche, T. Lee: Appl. Optics (2014)
plasma-torch stabilized CH₄/air flame



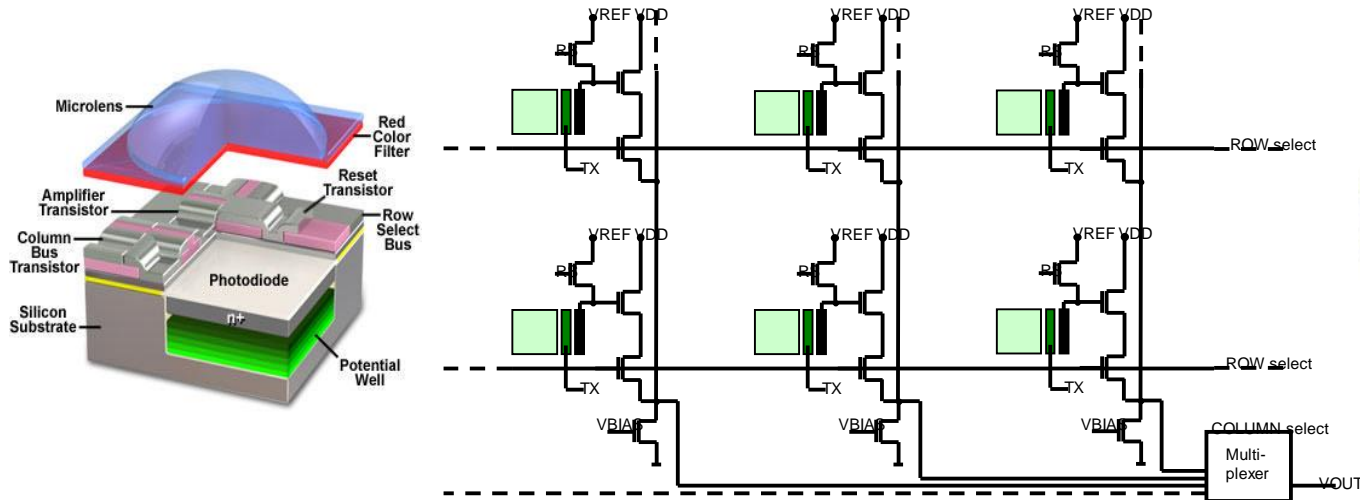
Instrumentation – cameras

- High speed cameras
 - Multi-frame CCD's cameras
 - Example: Princeton Scientific Instruments PSI 4
(28 frames, 3 MHz, 80x160 pixels, 14 bit)



Instrumentation – cameras

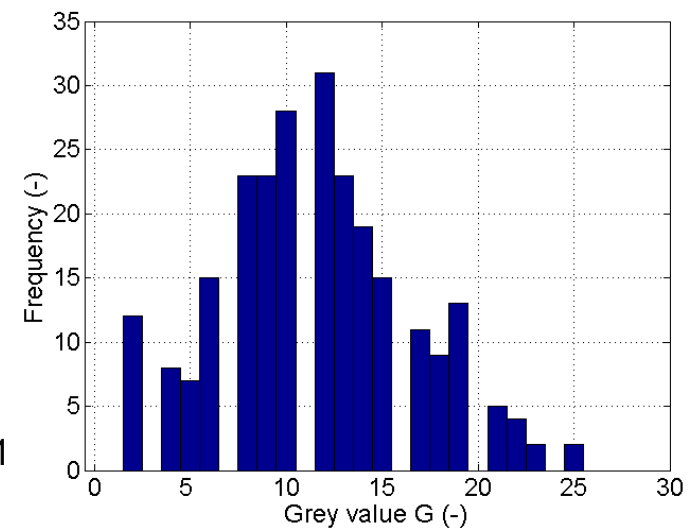
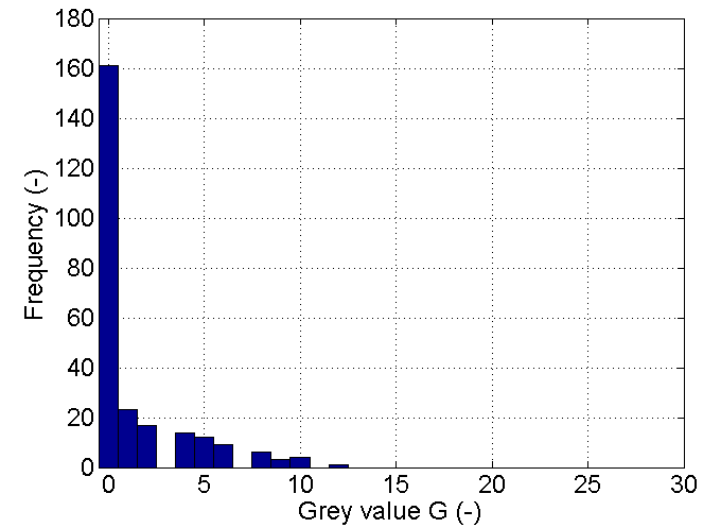
- High speed cameras
 - Multi-frame CCD's cameras
 - CMOS cameras
 - Example: Phantom v2512
(1280 x 800 @ 25,000 fps, 128 x 16 pixels @ 1,000,000 fps)
 - Other providers: PCO, Photron



Photron

CMOS – basic sensor checks

- High speed CMOS not yet temp. stabilized
 - Significant temperature drift, independent on illumination
 - Wait for thermal equilibrium
- Truncated dark noise with “intensity calibration”
 - Switch off intensity calibration
- Vacancies in grey value resolution due to pixel gain
 - Reduces dynamic range
 - Introduces larger digitization noise



Weber, Dreizler APB 2011

CMOS – Non-linearity

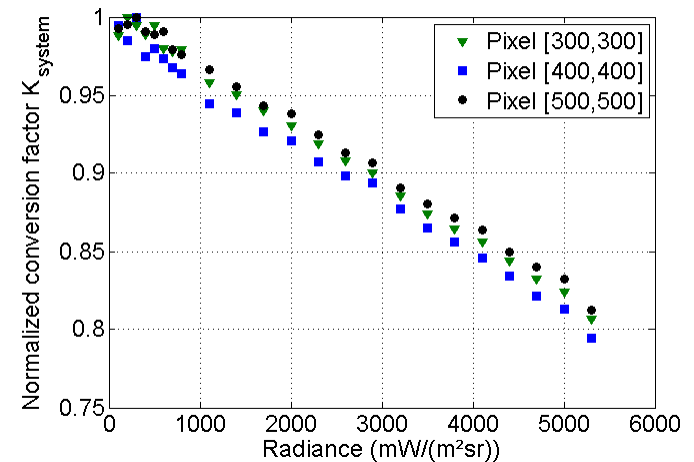
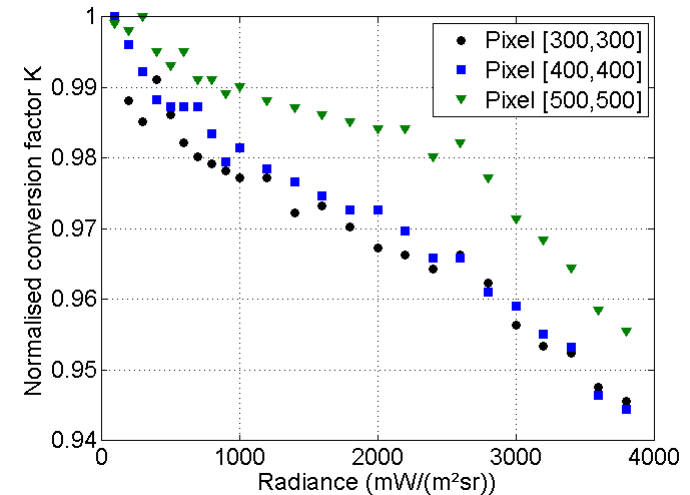
- Checking camera response (pixelwise)
→ Homogenous calibrated light source
(Ulbricht sphere)

- Model for pixel response as

$$G_i = G_{0,i} + K_{i,N_{e,i}} N_{e,i}$$

- Inherent non-linear response
- Deviations from linearity < 6%

- Inclusion of image 2-stage-intensifier
(MCP + booster)
→ Significantly increased non-linearity



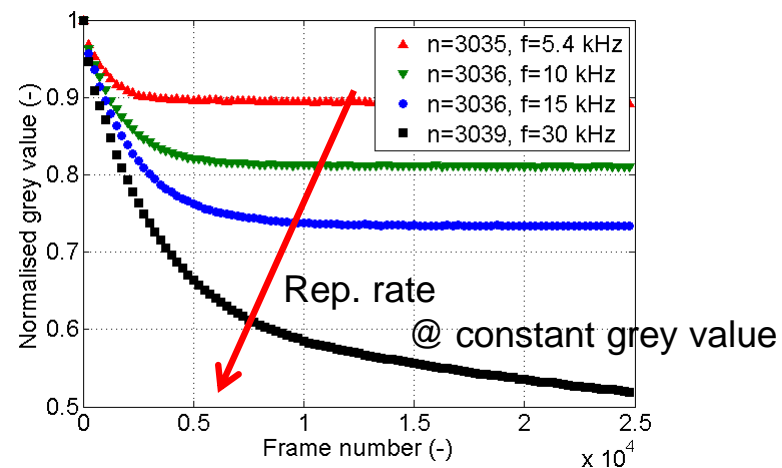
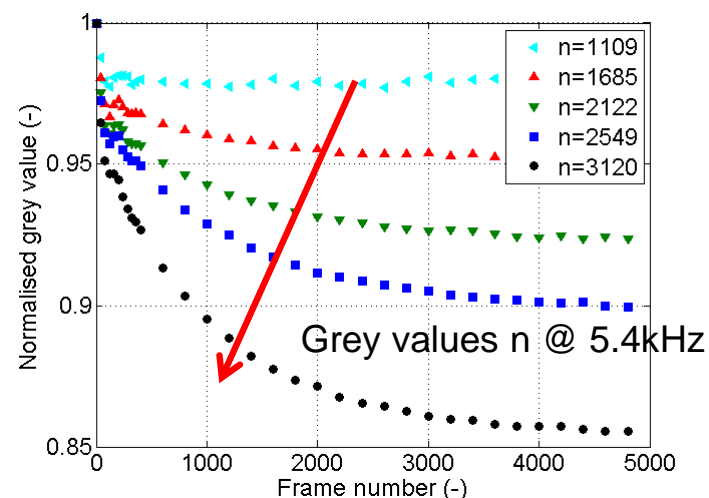
CMOS – image intensifier signal depletion

- Intensified systems suffer from signal depletion
- Full sensor illumination: Depletion increases with signal intensity (grey value n) and repetition rate

→ Without correction: device is unable to reproduce a constant signal within the first few 2000 frames

- Dependent on
 - Signal intensity
 - Frame rate
 - Exposure time
 - Illuminated area

→ In-situ calibration required



CMOS – quantitative measurements

- Unintensified CMOS camera (preferred)
 - Resolve dark signal (disable IC)
 - (Pixelwise) correction of nonlinearity

 - Intensified CMOS
 - Pixelwise correction of nonlinearity
 - Signal depletion. No best practice advice available
 - Solution: monitor depletion with spot of known illumination?
 - “Halos” (steep intensity gradients cause cross-talk to neighboring pixels)?
- Each CMOS camera/ intensifier has unique characteristics
- Need for common calibration procedure
- EMVA 3.0 not suitable for our needs

